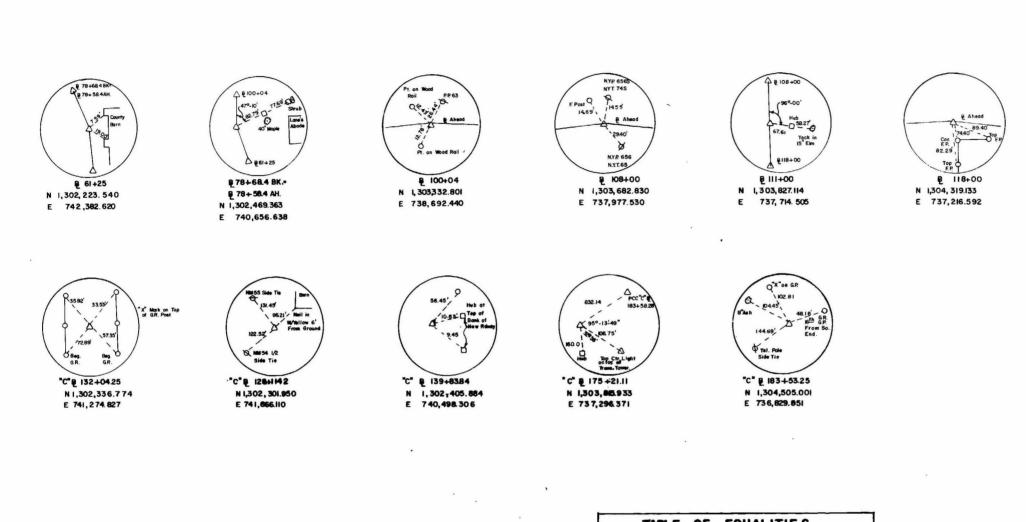


F A.R.C. 72-1

	×.	F-BRF- 371 (8)	9	3
SH 55	и 18 мн 16 г.	3.		
9 1.91	13 SOUTH 544			
SH .56	TA WHITEHA	5		

/				
AK > PAVT	aler.	to an		1 ^{,6} H
180	The S	CUNTY RUL	лте у	\$
10 ST ELVOS	2000 000 000 000 000 000 000 000 000 00	JALS DER		St. J. F. J. J. J. St. W. A.
A A A	C _L MILES	LANA MILES	ZZ AGENCY	Adrated Maint. Jurisdictic.
ED	(CONT'D.)	1	×	
HT	0.15	0.30	WASH. COUNTY	SECT. 62, HIGHWAY LAX & RESOLUTION DATED 9/20/7
<u>0</u> <u>N</u>	SIRUQ	ZILON	<u>l</u> ·	
	0.06	0.12	STATE	SECT.62, HIGHWAY LAS SECT.62, HIGHWAY LAS
	0.06	0.12	STATE	SECT. 62, HIGHWAY _A.
	0.13	0.26	STATE	SECT. 62, HICHWAY YAW
<u>A L</u>				
5	0.31	0.62	STATE	SECT. 12, HIGHWAY LAW
	0.27	0.54	STATE	SECT. 12, HIGHWAY LAW
	0.39	0.86	STATE	SECT. 12, HIGHWAY LAW
,12			WASH. COUNTY	SECT. 12, HIGHWAY LAW

VILL.OF SECT. 10, SUBDIV. 27 WHITEHALL HIGHWAY LAW AND RESULUTION DATED



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_		BENCH	MARK	DATA
B.M. NO.	ELEV.	STATION	OFFSET	DESCRIPTION
SE	181.87	125+25	80' RT.	S.W. COR. GAS PUMP FOUNDATION
9B	102.81	C 145+50	100' LT.	BOLT IN 16" ELM
11X	105.85	C 168+00	75' LT.	BOLT IN 24" ELM
11B	156.62	C 180+45	75' LT.	BOLT IN POLE NM 671

TABLE OF EQUALITIES								
	-	COORDINATES						
C STATION	B STATION	NORTH	EAST					
C131+50	. C131+50							
P.C. C133+55,5	C133+55.5	1,302,350.186	741,124.127					
C146+50.24 =	C146+50.24=							
C147+00.00	C147+00.00	1,302,678.954	739,878.220					
P,T,C 1 46+00. 90	C146+12.13=							
	C146+00.98	1,302,659.103	739,923.297					
P.CO 166+88.97	C166+88.97	1,303,480.559	738,057.937					
PCC C183+09.40	183+53.25	1, 304, 505.001	736,829.851					

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* *.

STAT ION C128+11. C132+04. C139+83.8 C146+12.1 BK = AH C146+00.9 C146+50.2 BK = AH C147+00. C175+21. C183+53. 61+25 78+68. 78+58. 100+04 108+00 111+00 118+00 120+00 121+90

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F.A.R.C. 72-1
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				F.A.F	LC.	72-1
	ED. ROAD REG. NO.	STATE		ML AID SCT NO.	SHEET NO.	TOTAL SHEETS
	1	N.Y.		- 371 (8)	10	33
S	.H.5578	3 WHITE	HALL-DRES	DEN CENTER	PART 1	
S	.H.9113	3 SOUTH	BAY BRID	GE		
S	ASHING	7A WHIT	EHALL-DRE	SDEN CENTER	R PART	2
FE() 41.09' 2 Almont 0+00 H88-176 109-708						
SE	LIN	E	ATA		_	
	DISTANCE		COORDINAT	ES	-	
					_	

		Steel School St. Series	PORTAGE ACCOUNTS IN	
		DISTANCE	COORDI NAT	ES
	AZIMUTH	FEET	NORTH	EAST
.42			1,302,301.950	741,666.110
. 25	275-05-09	392.83	1.302.336.774	741.274.827
.84	275-05-09	779.59	1,302,405.884	·
	293-46-03	628.29	1, 502, 405.004	740,430.300
.13 H .98			1,302,659.103	739,923.297
. 24	29 3-46-03	49.26		
H .00			1,302,678.954	739,878.220
.11	293-46-03	2821.11	1,303,815,933	737, 296. 371
. 25	325-54-03	832.14	1,304,505,001	736 829 851
. 27			1,302,223.54	
. 4BK	278-06-21	1743.40	1,302,469.363	740,656.638
	293-43-47	2145.60	1.303.332.801	738 692 440
	296 - 05-13	796.00	1,303,682.830	
	298-44-50	300.00	1,303,827.114	
	314-39-32	700.00		
	327-41-43	200.00	1,304,319.133	
	327-42-05	190.00	1,304,488.176	
			1,304,648.779	737,008.185

BASE LINE & BENCH MARK DATA

BC 45 (8-76)

BOX	BEAM	GUIDE	RAIL			
STATION TO STATION	SIDE	ITEM 33AF ACTUAL LE	ADJUSTMENT FACTOR	ITEM 33AF LE	I TEM 33AFY LE	ITEM 33AFDR EACH
C130+80 - C134+5G C149+56 - C151+88 C149+56 - C151+88 C157+27 - C162+44 C157+27 - C162+44	L T. LT. LT. LT.	226 105 55* 55* 390	1.0 1.0 1.2 1.2 1.0	226 105 66 66 390	144 72 - 72	- 2 1 - 1
C132+16 - C134+50 C145+80 - C151+ 88 C157+2 7 - C169+22	RT. RT. RT.	96 536* 1123*	1.0 1.2 1.2	96 643 1347	144 72 +72	2 1 1
*INCLUDES 5' CONNEC- TION TO BRIDGE		TOT	ALS	2939	576	8

.

CABLE	GUIDE	RAIL		
STATION TO STATION	SIDE	ITEM 32 DH LF	ITEM 32 DOD EACH	
C167+00-C171+00	LT.	400	2	
<i>C</i>	TOTAL	400	2	

RESETTING GUIDE RAIL						
STATION TO STATION	SIDE	ITEN 32R LF				
C181+85-C183+09.43	RT.	125				
	TOTAL	125				

		UTILITY	DISPOSITION T	ABLE				
TABULATION OF UTILITIES								
STA. TO STA	SI DE	OWNER	DESCRIPTION	. DISPOSITION	STATUS OF AGREEMENT			
C130+75 C183+09 .43	L & R	NIAGARA MOHAWK POWER CORP.	OVERHEAD POWER	NOT AFFECTED				
C130+75 C144+85	L	NEW YORK TELEPHONE	OVERHEAD TELEPHONE	NOT AFFECTED				
C 144+85 C 163+20	L&R	NEW YORK TELEPHONE	OVERHEAD TELEPHONE LINES	TO BE RELOCATED BY OWNER (4" CONDUITS IN SOUTH BAY BRIDGE	OWNER AGREED TO RELOCATE			
C163+20 C183+09.43	L&R	NEW YORK TELEPHONE	OVERHEAD TELEPHONE	NOT AFFECTED				
C 1 30+75 C 1 42+15	R	VILLAGE OF WHITEHALL	UNDERGROUND WATER					
C142+15 C169+91	R	VILLAGE OF WHITEHALL	UNDERGROUND WATER MAIN	TO BE RELOCATED ON TO PROPOSED STRUCTURE IN CONTRACT				
C169+91 C183+09.40	R	VILLAGE OF WHITEHALL	UNDERGROUND WATER					

	TABLE	OF	LENGTHS		a a=a a
DESCRIPTION	STATION TO	STAT ION	DESCRIPTION	LE	MILES
CONTRACT BEGINS	! 30+75 -	C131+50	PROJECT BEGINS	75	0.01
PROJECT BEGINS	C131+50 -	C146+50.24=	EQUALITY	1500.24	0.28
EQUALITY	C147+00 -	C148+60	VILLAGE LINE OF WHITEHALL S.H. 5578 ENDS	160	0.03
TOWN LINE OF WHITEHALL S.H. 9113 BEGINS	C148+60 -	C151+87.86	BRIDGE BEGINS	327.86	0.06
BRIDGE BEGINS	C151+87.8	6-C157+27.14	BRIDGE ENDS	539.28	0.10
BRIDGE ENDS	C157+27.1	4-C157+35	TOWN LINE OF WHITEHALL	7.86	0.00
TOWN LINE OF DRESDEN	C157+35 -	C163+00	S.H. 9113 ENDS	565	0.11
S.H. 5736A BEGINS	C163+00 -	C183+09.46	PROJECT & CONTRACT END	2009.46	0.38
INTERSECTING ROAD D (M, STA. C145+49)	D 0+12 -	D 1+60	LIMIT OF WORK	148	0.03
INTERSECTING ROAD E (M. STA. C171+15)	E 0+12 -	E 1+40	LIMIT OF WORK ·	128	0.02
COUNTY ROAD 7 (M. STA, C181+15)	0+12 -	0+70	LIMIT OF WORK	58	0.01
	ENGTH 1660.24	4 L.F. = 0.31 M	ILES (VILLAGE OF WHITEHALL)	
S.H. 9113 PROJECT L	ENGTH 1440.00	D L.F. = 0.27 M	ILES (TOWNS OF WHITEHALL &	DRESDEN)	
S.H. 5637A PROJECT I	ENGTH 2009.4	6 L.F. ≈ 0.38 M	ILES (TOWN OF DRESDEN)		
CONTRACT I	ENGTH 5184.7	0 L.F. = 0.98 M	ILES (WASHINGTON COUNTY)		

EARTHWORK SUMMARY		ITEM 2A EXCAV. & DISPOSAL OF EXCAV. MAT'L CUYD.	ITEM 2 62 Embankment In place Cu. yd.	ITEM 2ECBGI SELECTE D BORROW CU. YD.	ITEM 2EF B SELECTED GRANULAR FILL CU. YD	I TEM 2VJE SELECTED FILL (BRIDGE FOUNDATION) CU. YD	ITE58 STRUCTURAL EXCAV- CU.YD.	ITEM 5T TRENCH & Culvert Excàv. Cu.yd.
EXCAVATION FROM EARTHWORK SUMMARY SHEET Excavation from drainage sheet Excavation from water main sheet Quantities from bridge summary sheet Total combined neat	NEC.	14,391	41,222	12,647	564	553	508	101 1,063

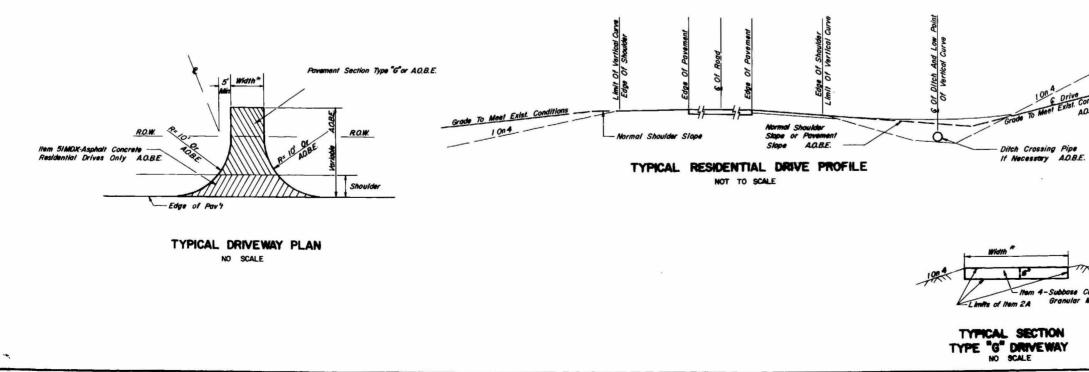
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F.A.R.C. 72-1

FED. NOAD NES. NO.	STATE	FEDERAL AID PROJECT NO.	SHEET NO.	TOTAL SHEETS
1	N.Y.	F-BRF- 371 (8)	п	33
SH 913	OUTH BAY	DRESDEN CENTER PA BRIDGE DRESDEN CENTER PAR		
WASHINGTO	ON COUNT	Y		

MISC. TABLES

C CTATION	CIDE	TYPE	WIDTH	CULVE	RTS	0	ULVERT OF	FFSETS	
C STATION	SIDE	TYPE	L.F.	SIZE (IN)	ENGTHILF	STATION	OFFSET	STATION	OFFSET
C 134+65	RT.	G	12						
C 135+34	LT.	G	12						
C 137+00	RT.	G	12	1 2"	24 '	C 136+85±	34'RT.	C 137+15 <u>+</u>	35'RT.
C 137+38	LT.	G	12	12"	30'	C 137+23±	37'LT.	C 137+53 <u>+</u>	37'LT.
C 137+58	RT.	G	12	12"	28 '	C 137+44 <u>+</u>	36'RT.	C 137+72 <u>+</u>	35'RT.
C 143+50	LT.	G	12	12 '	34'	C 143+36 <u>+</u>	40'LT.	C 143+70 <u>+</u>	40'LT.
INT. RD. D	RT.			12"	54	C 145+24+	31'RT.	C 145+82 <u>+</u>	40'RT
C 166+70	LT.	G	12	24"	72:	C 166+34 <u>+</u>	53'LT.	C167+06±	50'LT.
INT. RD. E	RT.			24.	142'	C 170+43±	64'RT.	C171+88 <u>+</u>	80'RT
C 174+90	LT.	G	12	12	44 '	C 174+67 <u>+</u>	37'LT.	C175+11 <u>+</u>	34'LT
D 1+15	RT.	G	12'						
E 1+40	RT	G	24						



PONTON SALE TO BE MANTELLES APTROPRIST

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F.A.R.C. 72-1

FED. ROAD REG. NO.	STATE	FEDERAL AND PROJECT NO.	SHEET NO.	TOTAL
1	N.Y.	F-BRF- 371 (8)	12	33
S.H. 5578	WHITEHAL	L- DRESDEN CENTER	PARTI	
S.H. 9113	SOUTH B	AY BRIDGE		
S.H. 5637A	WHITEHA	LL-DRESDEN CENTER	PART 2	
WASHINGTO	N COUNT	1		14 - A

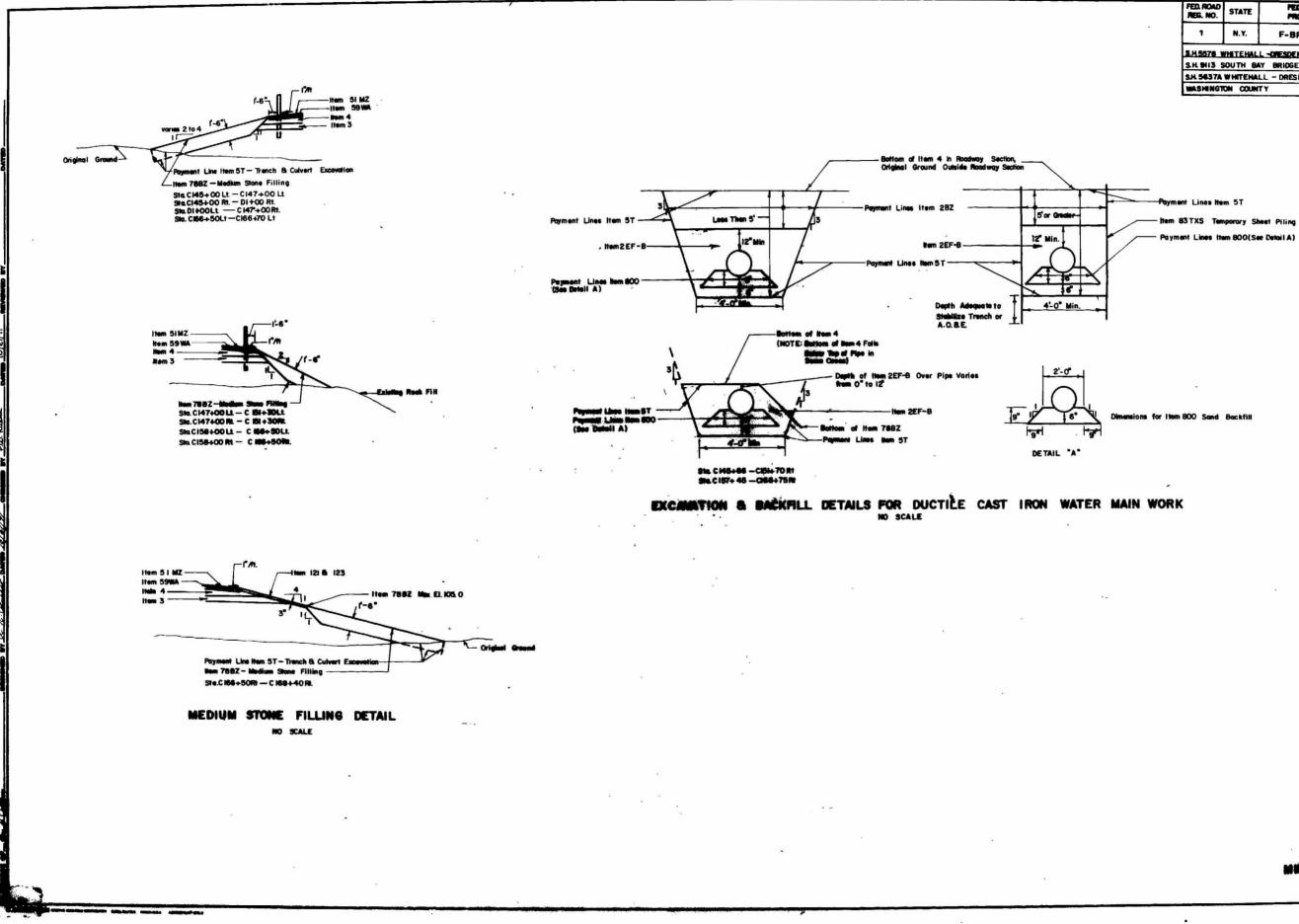
DRIVEWAY CULVERT NOTES: The Above List Of Driveways is intended For Estimate Purposes Only. The Exact Number, Location And Width Of Placement Will Be Determined By The Engineer. All Driveway Pipe To Be Item 14 MQ, Optional Culvert Pipe, With Item 14 ESM, Optional End Section, At Each End Unless Otherwise Noted On Plans Or Ordered By The Engineer.

Item 4-Subbase Course Select Granular Material-6

NOTE: All Drives Shall Conform To "Policy Arid Standards For Entrances To State Highways" As Adopted July 1,1960. * As Shown On Toble Or A.O.B.E.

DRIVEWAY DETAILS

HC 476 (9/90)

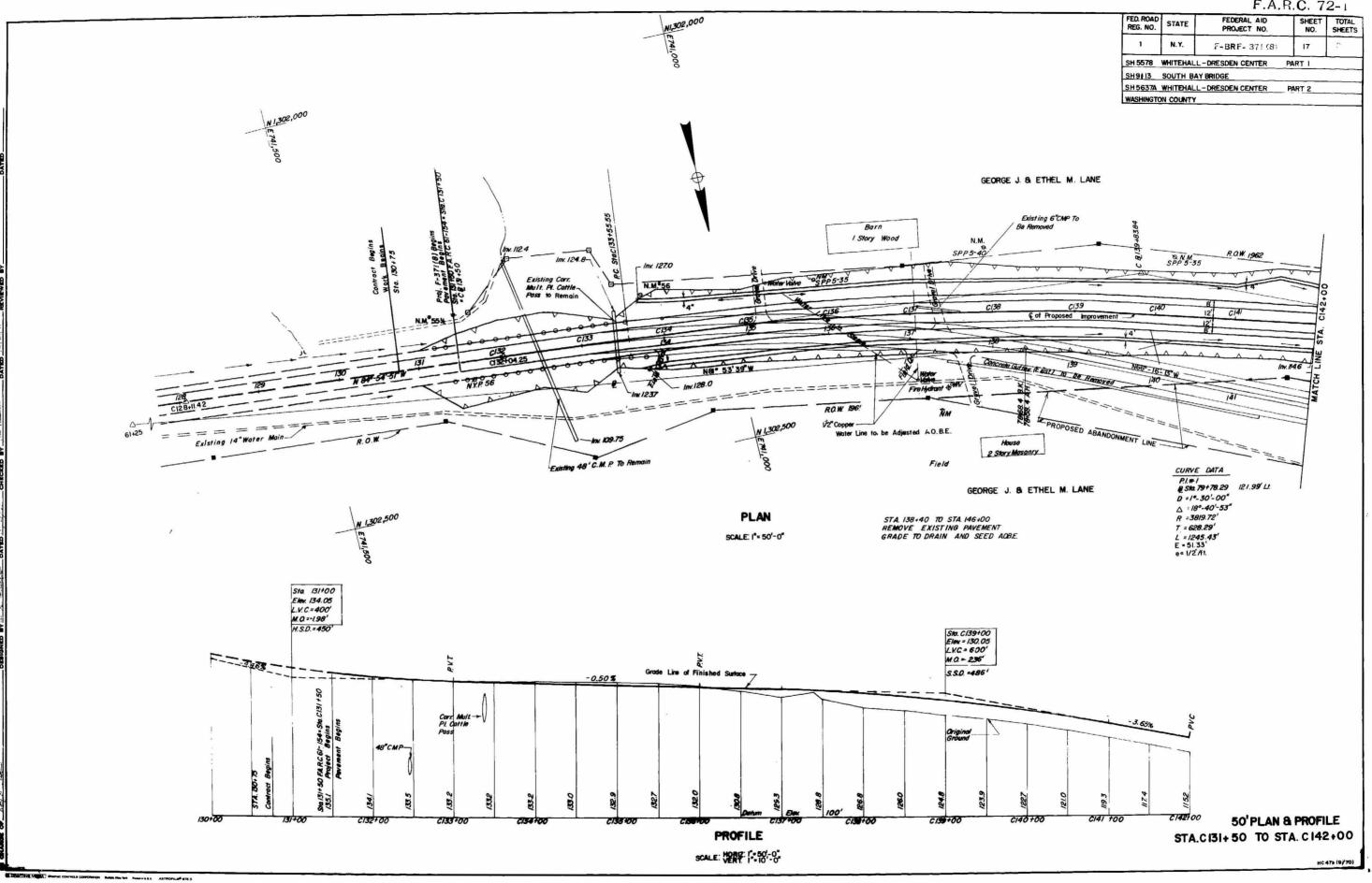


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ł.л,	n.c.	72-

FED. ROAD REG. NO.	STATE	PEDERAL AID PROJECT NO.	SHEET NO.	TOTAL SHEETS
1	N.Y.	F-BRF- 371 (8)	14	33
S.H. 5578 V		ORESDEN CENTER PA	RT	
SH 5637A	WHITEHAL	- DRESDEN CENTER	PART2	
WASHINGT	THE COLUMN	Y		

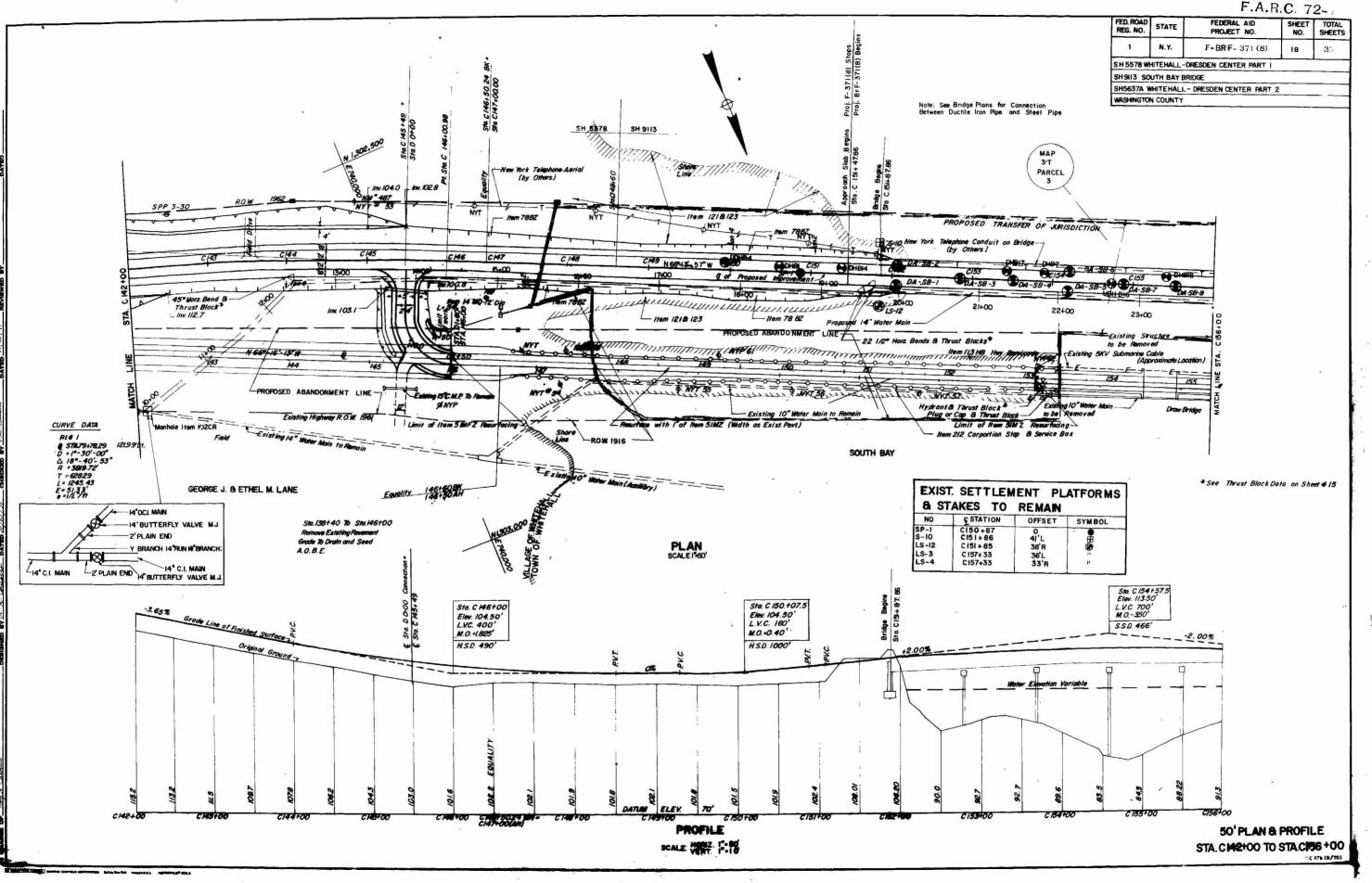
MINC. DETAILS





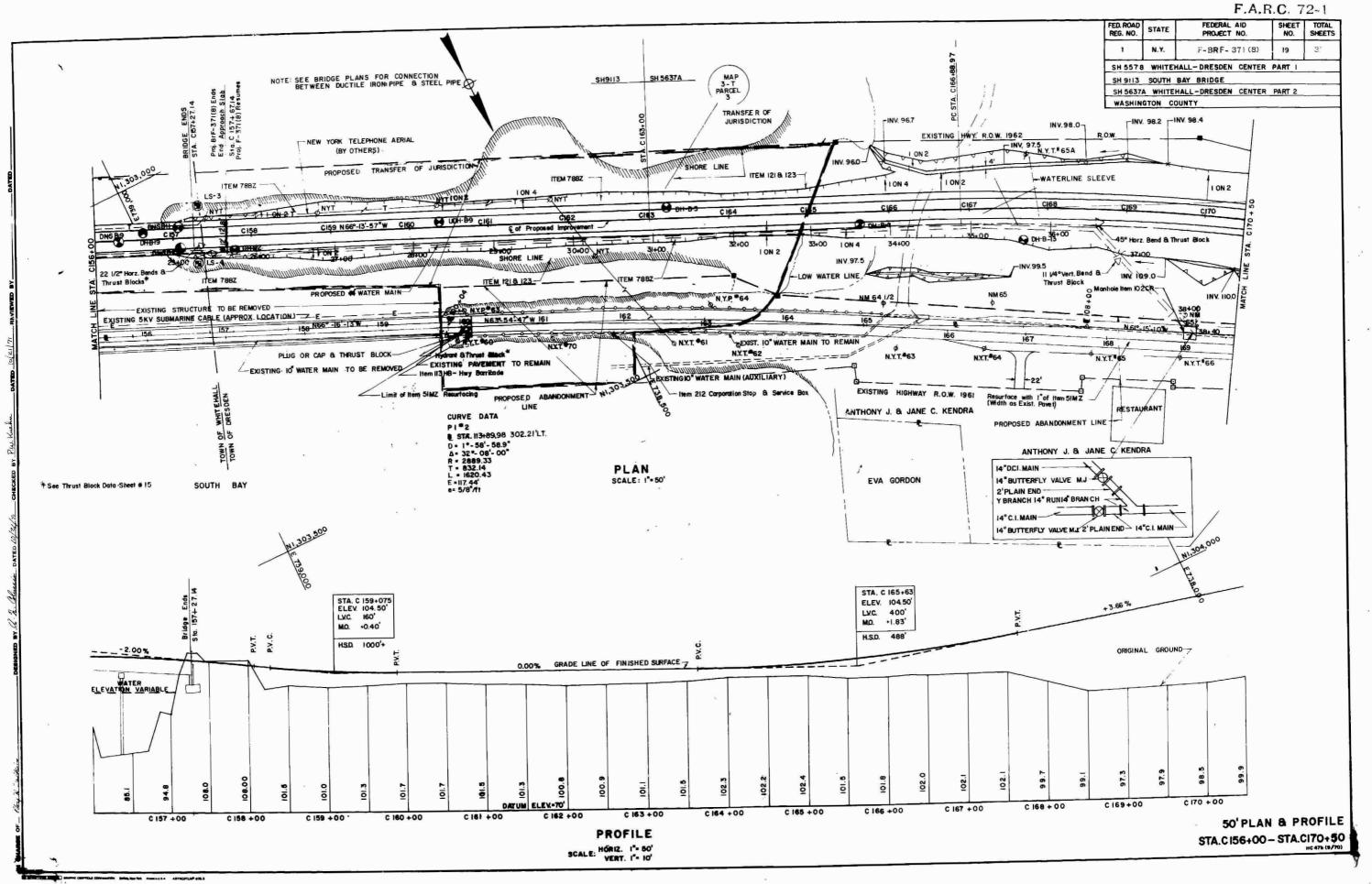
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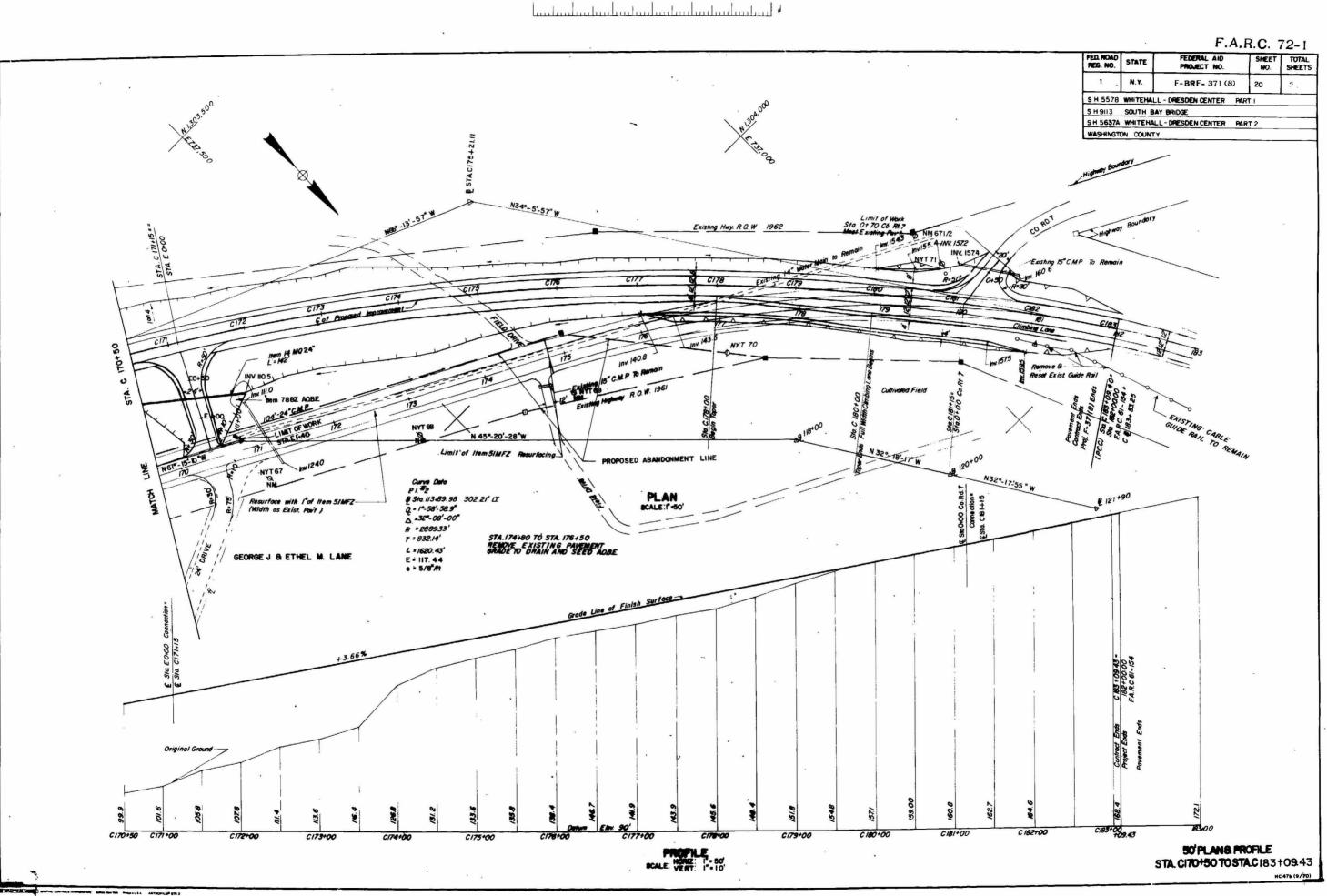




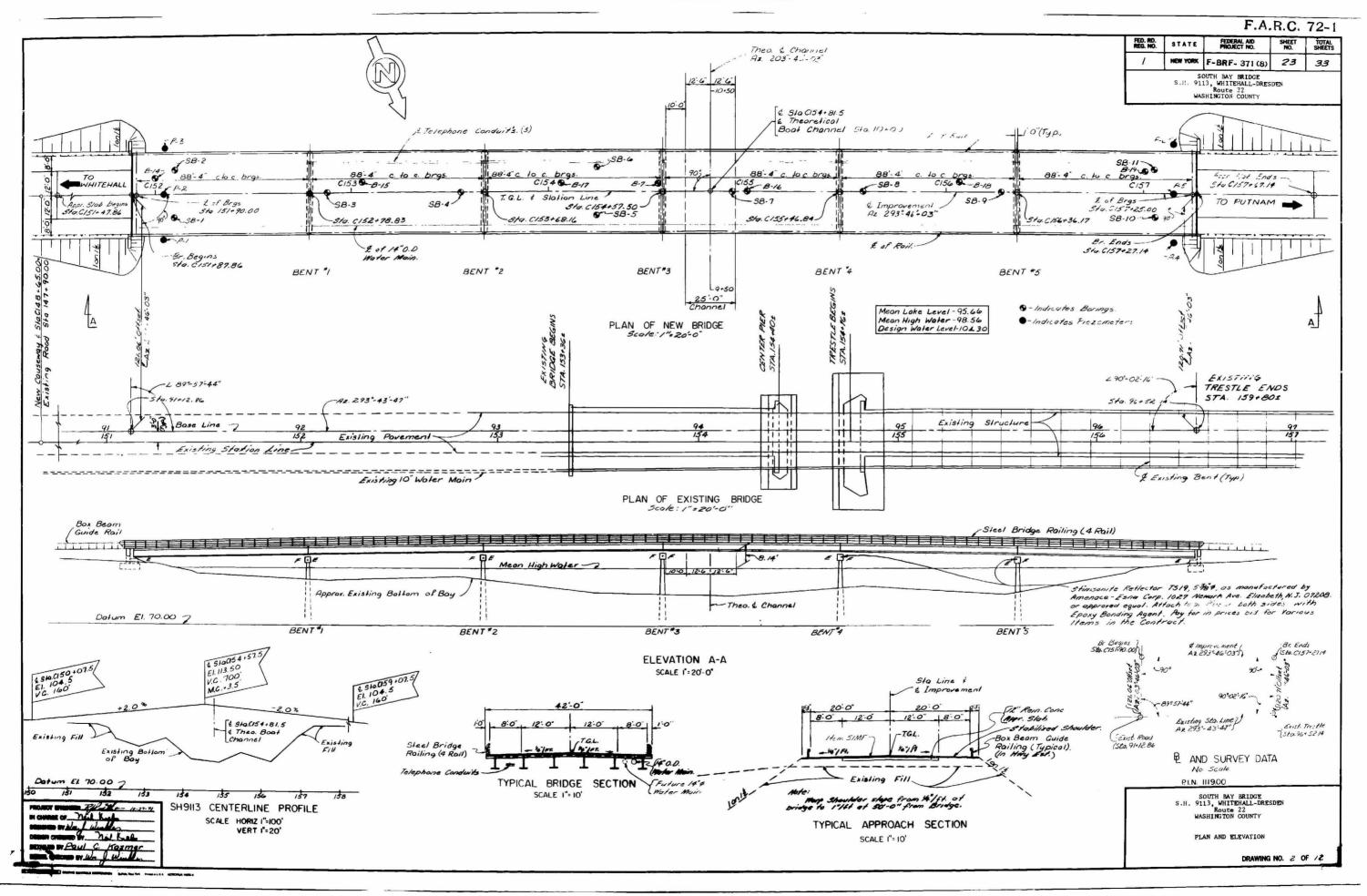
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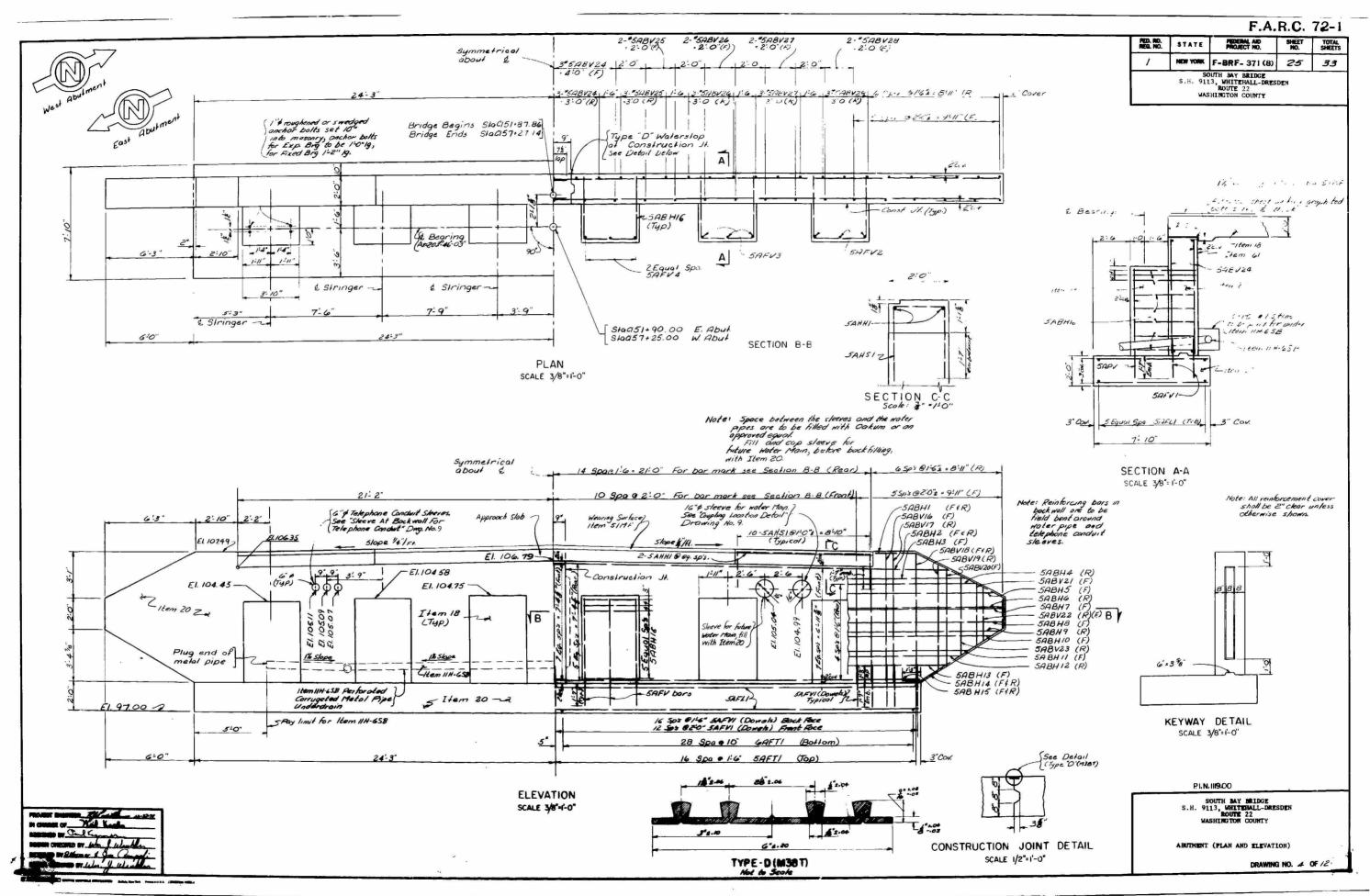




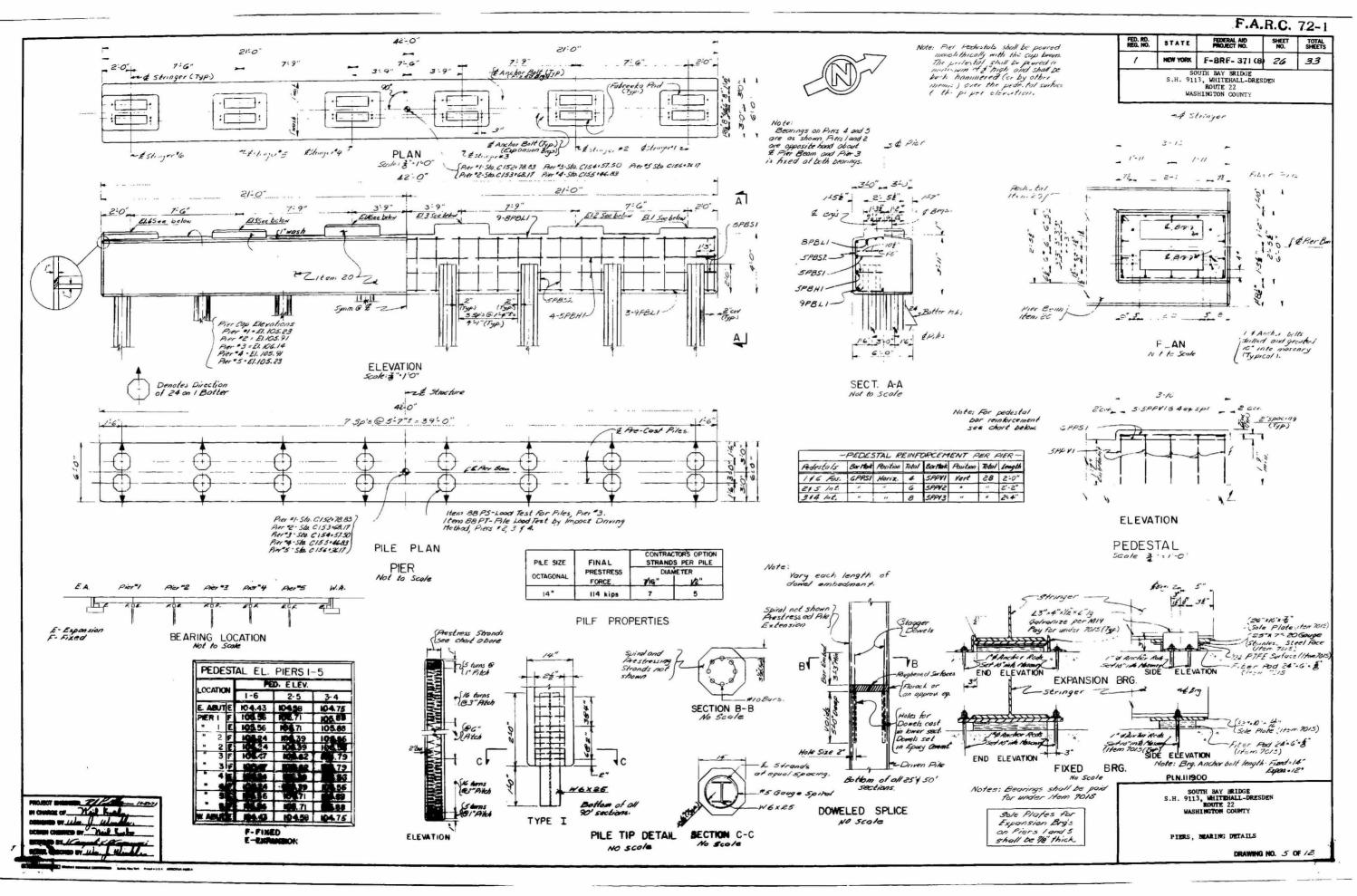


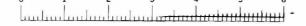


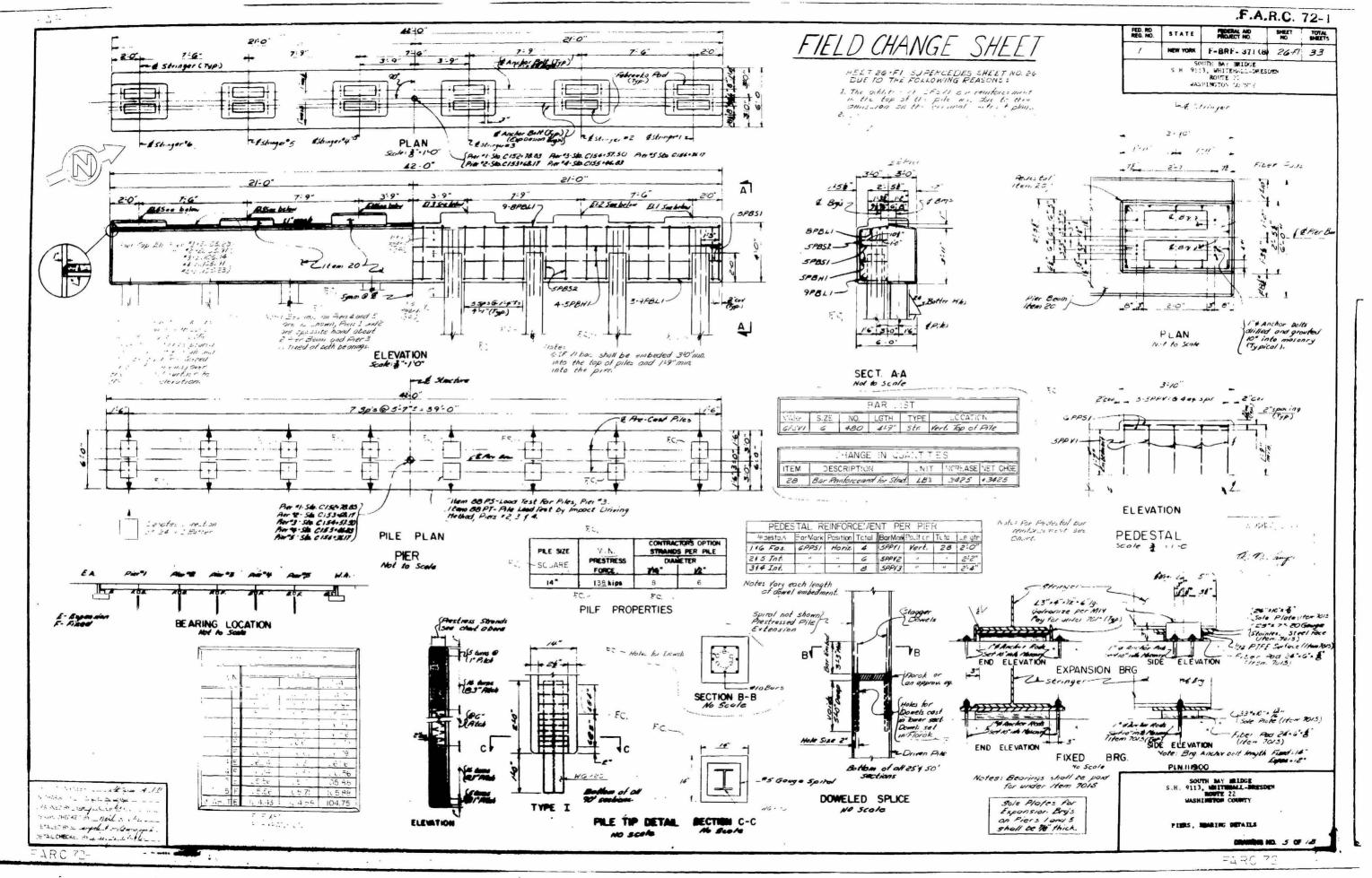
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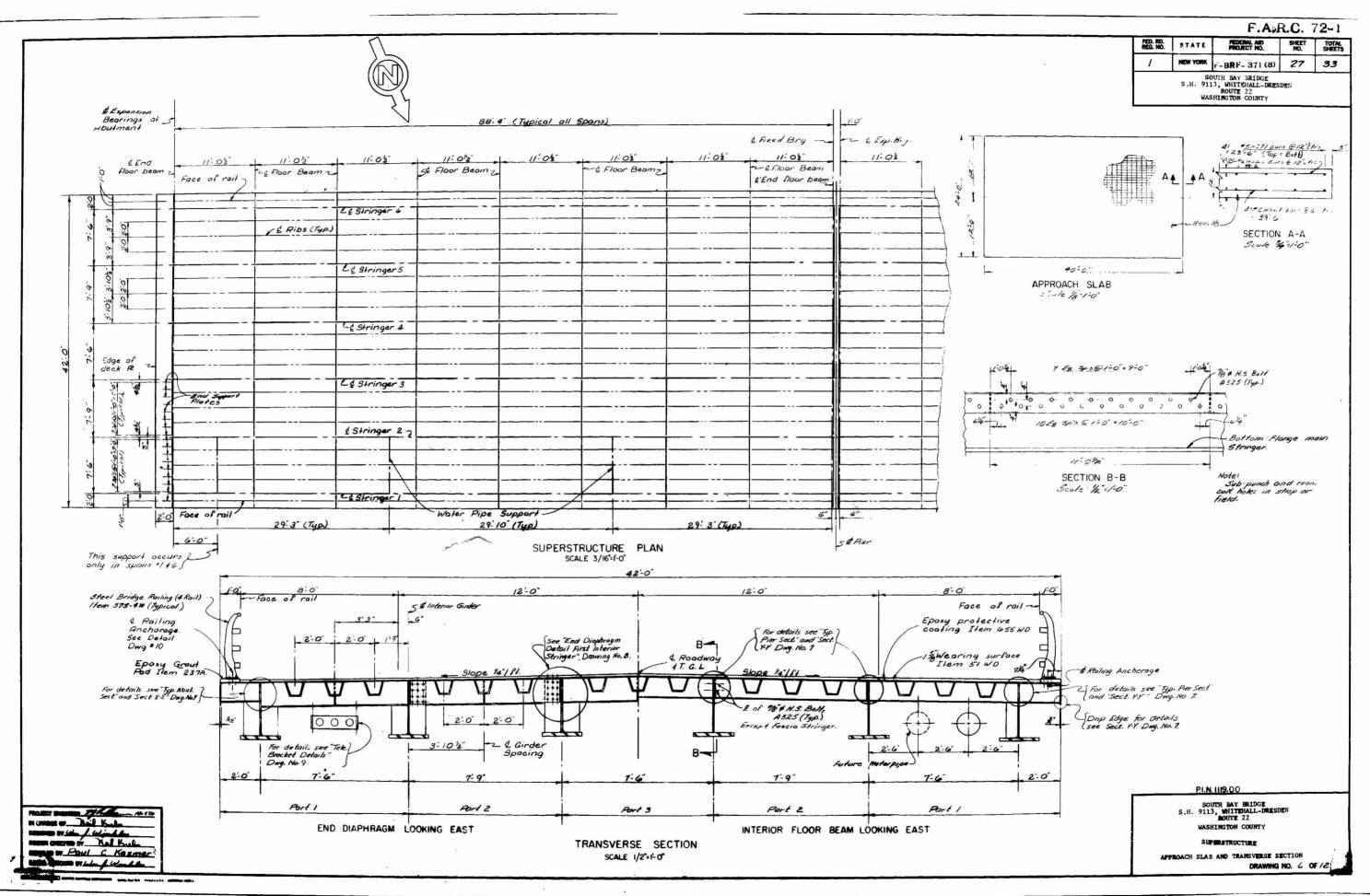
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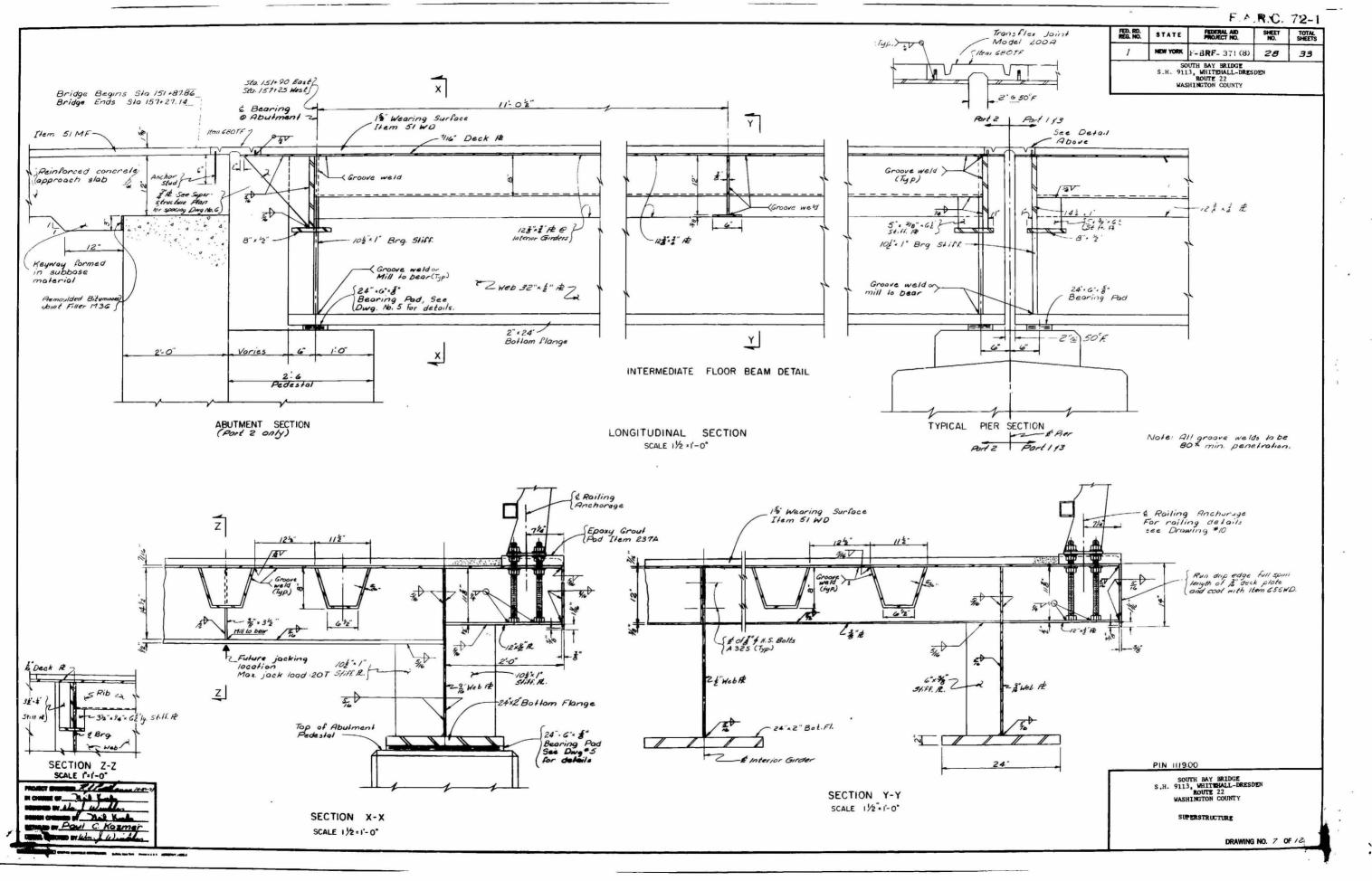




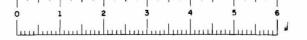
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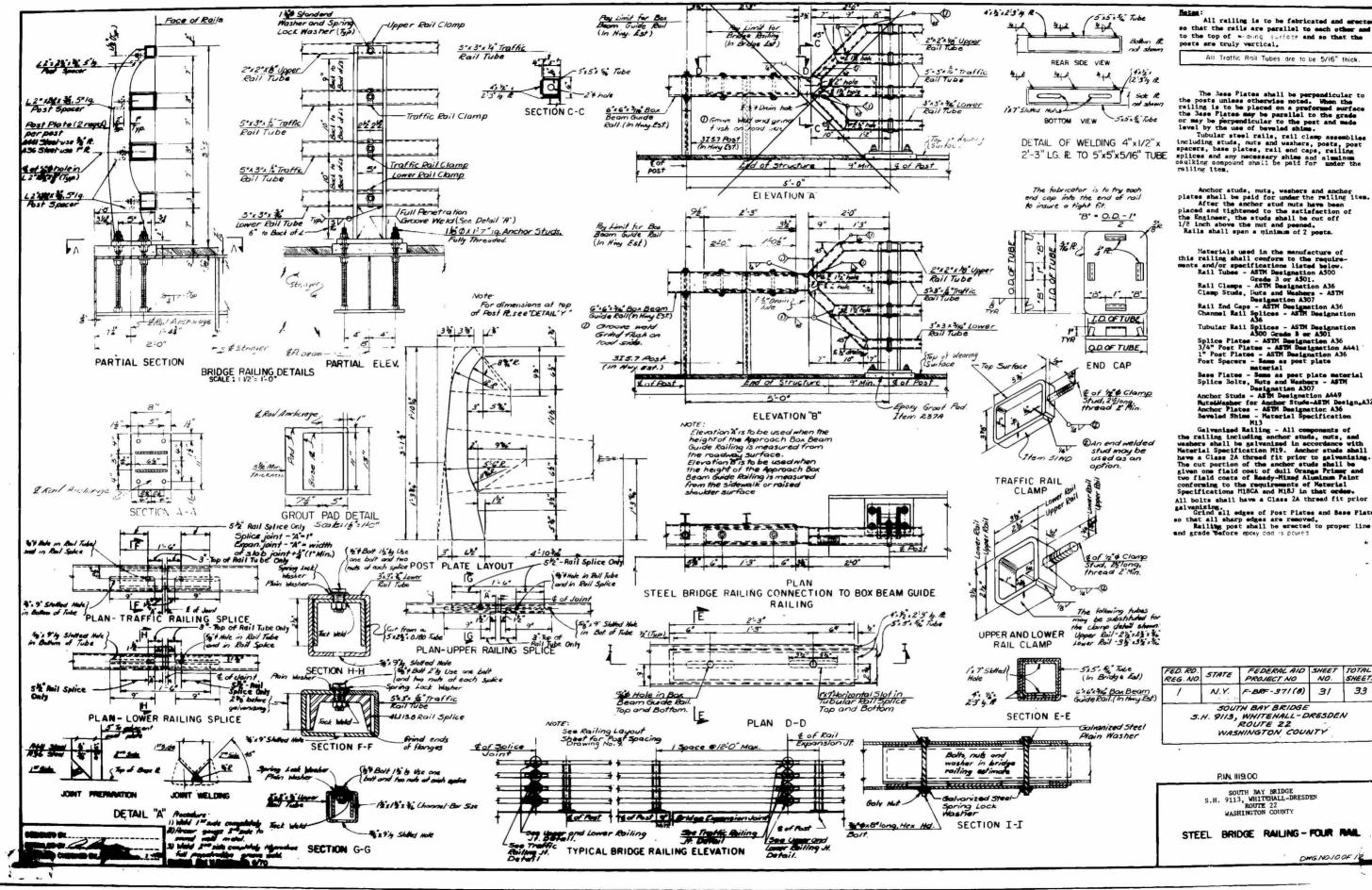






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All railing is to be fabricated and erect so that the rails are parallel to each other and to the top of woung surface and so that the posts are truly vertical.

All Traffic Rail Tubes are to be 5/16" thick.

Anchor studs, muts, washers and anchor plates shall be paid for under the reling item. After the anchor stud muts have been placed and tightemed to the satisfaction of the Engineer, the studs shall be cut off 1/2 inch above the mut and peened. Rails shall span a minimum of 2 poets.

Materials used in the manufacture of this railing shall conform to the require-ments and/or specifications listed below. Rail Tubes - ASTM Designation A500 Grade 3 or A501. Rail Clamps - ASTM Designation A36 Clamp Stude, Nuts and Weshers - ASTM Designation A307 Rail End Caps - ASTM Designation A36 Channel Rail Splices - ASTM Designation A36 Tubular Bail Splices - ASTM Designation Altimet All splites - As it Designation ASO Tubular Rell Splites - ASTM Designation ASOO Grade B ser ASOI Splite Plates - ASTM Designation A36 3/4" Post Plates - ASTM Designation A36 Post Spacers - Same as post plate material Base Plates - Same as post plate material Splite Bolts, Futs and Mashers - ASTM Designation A307 Anchor Studs - ASTM Designation A449 RuteHeader for Anchor Stude-ASTM Design.A322 Anchor Flates - ASTM Designation A36 Beveled Shims - Material Specification H13 M13 Gaivanized Railing - All components of the railing including anchor studs, muts, and washers shall be galvanized in accordance with Material Specification M19. Anchor studs aball have a Class 2A thread fit prior to galvanizing. The cut portion of the anchor studs shall be given one field coat of dull Orange Primer and two field coats of Ready-Mized Aluminum Faint conforming to the requirements of Material Specifications H18CA and M18J in that ecdes. All bolts shall have a Class 2A thread fit prior i M13 All bolts shall have a Class 2A thread fit prior All bolts shall have a Glass 24 thread it picts of galvanisme. Grind all edges of Post Plates and Base Plate so that all sharp edges are removed. Railing post shall be erected to proper line and grade before epoxy cod is poured FEDERAL AID SHEET TOTAL STATE NO. PROJECT NO SHEETS 31 33 N.Y. F-BRF-371(8) SOUTH BAY BRIDGE 5.H. 9113, WHITEHALL-DRESDEN ROUTE 22 WASHINGTON COUNTY P.I.N. 1119.00 SOUTH BAY BRIDGE S.H. 9113, WHITEHALL-DRESDEN ROUTE 22 WASHINGTON COUNTY

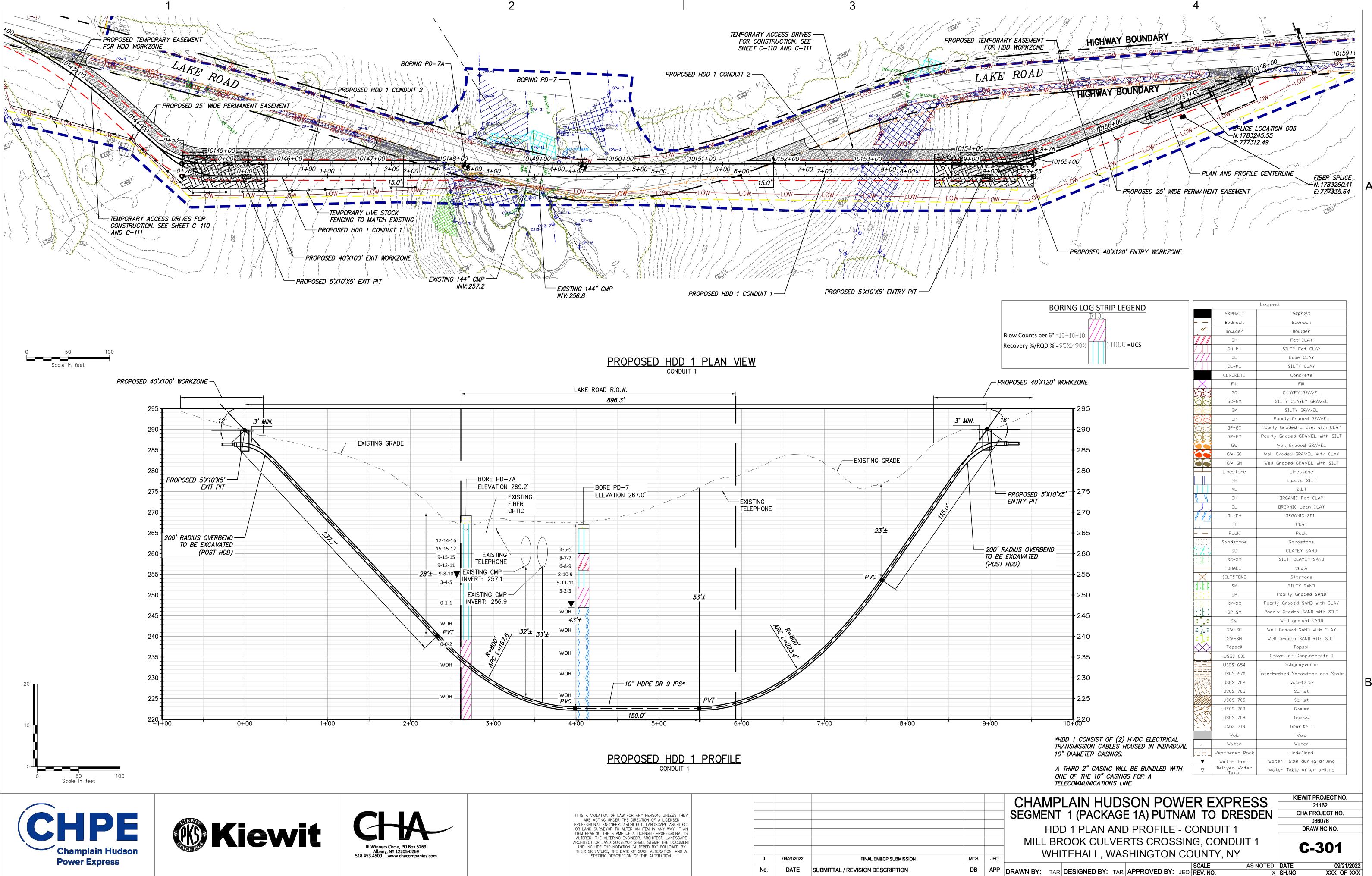
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MARK SIZE SPBNI 5 SPBSI 5 SPBSE 5 BPBLI 8 9PBLI 9 SPPVI 5 SPPII 6		L CHCTH	TYPE		T B		To		EI	GI			J	к	L	LOCATION	MARK	SIZE	NO	LENGTH	TYPE	A	B	Ċ	D	E	F	G
SPBSI 5	20	41-8	str.	-												Horiz in Pier Beam	· · · .	1			1							-
	20	8-0	IV	1-3	5-6	143		L								Stirrups in Pier Beam Bis	14	1		<i>*</i> -	+ ·					<u> </u>		
5PBSE 5	150	1912	TX	3-8	5-8	5±"	2:10	5-18"	5#"			-+	-+	-		Stirrups in Pier Beam		+					-					
8PBLI 8	65	41-8"	Str.				-			- +	+	-+				Long. In Pier (тор) " " (Bot.)												
5 POVI 5	13	210'	X	119	4"	1										Vert. in Pier Beam under Pedestal												
SPAVE 5	140	212	"X	1411"	4"											11 11 11 11 11 11 11 11 11 11 11		-					-					
SPPV3 5	140	213	" <u>X</u>	2-1"	4"	-3"	-11				-+					Heriz. in Velestel		-										
GPPSI G	190	11-9"	12	3-6	2-12	57	22				-	-	- 1	_		HONE. M FESSARN						-				-		
	1				1										Ľ			_				-						
						ΔF	PRCA	CH S	SI AB								1								-			
	1	22/1		1		1	1	T				- 1	-			Trans in Approach shit Topfact.	-	+			+		-					
SHSTI 5 GHSLI 6	104	23-6	SIF								-					Long. in Approach slab Tops For												
CASEL 0	140	320						1						_												-		
					-			1											-	-			1-1					
						A	BUTM	ENTS									i	+	-			1	+					+
SAFLI 5	24	48:0	"iste	1	1	1	1			1	1					Abut. Ft. Long. (Tr'B)											<u> </u>	1-
SAFTI 5	66	714	str.													Abut Fly, Long. (T5'B) " " Trans Tip " " Bot.												-
GAFTI 6	116	744	571					-			-+					" " Bot.												
	1-		+	+		-				+	-+						1	1-1			1	1						-
SABHI 5	8	10'.7'	XXIII	2-8	6-1	68	1-10	2:9								Abut. Bockwall Horiz (FER)												
SABNE 5	8	26-3	str.	1												(F¢R)*												
3	4	27-3'	+	+	1	-					-+					(F 1R) (R)		+	-	-	-							+
4	++	29-0	•	t	-	-	+		- +		-+	-+	+													1		1-
6		29: 9														(R)												
7		29'-9"														(F)				-								
8		29-9		+								-+	-+			(F) (R)		+ - +						-				+
N.		29'-0"	TT	1 -												(K) (F)												1
11		27-6														(F)												
12	1-1-	27-0"	tat	+			ł						-+	_		(R)					- 1	-						
5ABH14 5	8	9.7	TXIII	143"	5-7"	6:1	1:10"	3'- 0'			+	-	-+			(F) (F¢K)		+								-		+
SARHIE 5	A	2422	J.Te.										_	-	_	A but Backwall Horiz (FEIR)												1
SARHIG 5	96	11: 7"	IL	4:2"	3'6	4-2"	1									Abut Backwall Horiz. into Padestal Abut Backwall Vart. (Front)						-						
5ABHIG 5 5ABVIG 5 17	4	8.4"	570	+			t				+					Abut Backwall Vart. (Front) (R)		+			-					-		-
18	8	8:4					L	1				+				(F¢R)						<u> </u>						
19	4	2'0"														(R)												
20				+												(F)												
21	4	4:0	++	1		t										(F) (F¢R)		+										+
23	4	5:3																1-1								<u> </u>	<u> </u>	
24	20	7:5			L								1			(FER)												_
	20			+	-						\rightarrow	- +			_	"												
27	20	7:2"					1	1			-+	-+				<i>H</i>		+			+		-			i		
5481 28 5			Ste				[t				Abut. Backwall Vert. (F. + R.)					1							
SAFUI 5	112	2510	44.			-					-																	
25	12	6-10		1	1		<u>+</u>	-			+		+			Abet. Ftg. Dovels		+										+
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	12	712"		1						11 A						•••• a												

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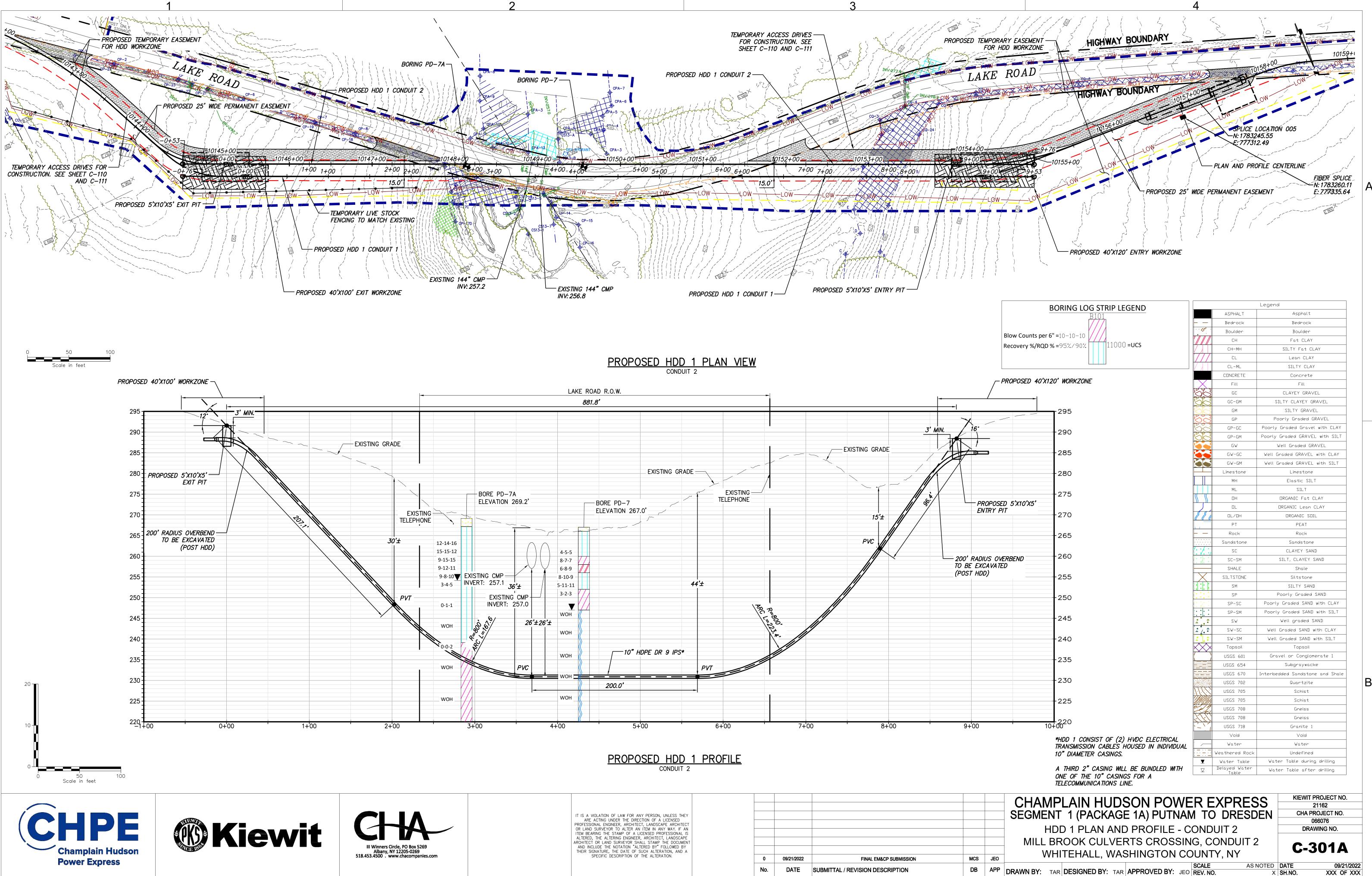
Appendix C

HDD Design Drawings

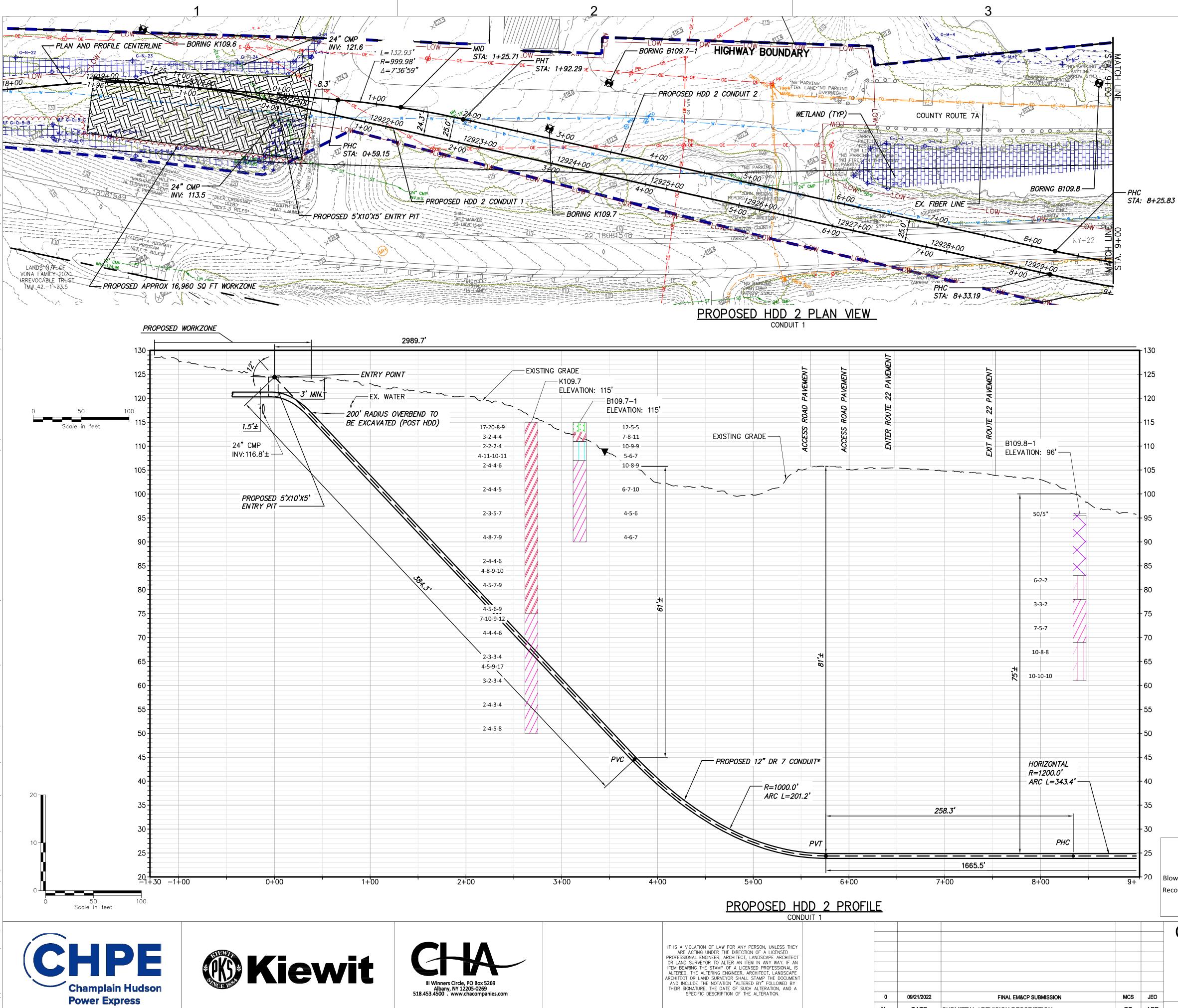


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PROPOSED HDD 2 PROFI	<u>LE</u>					
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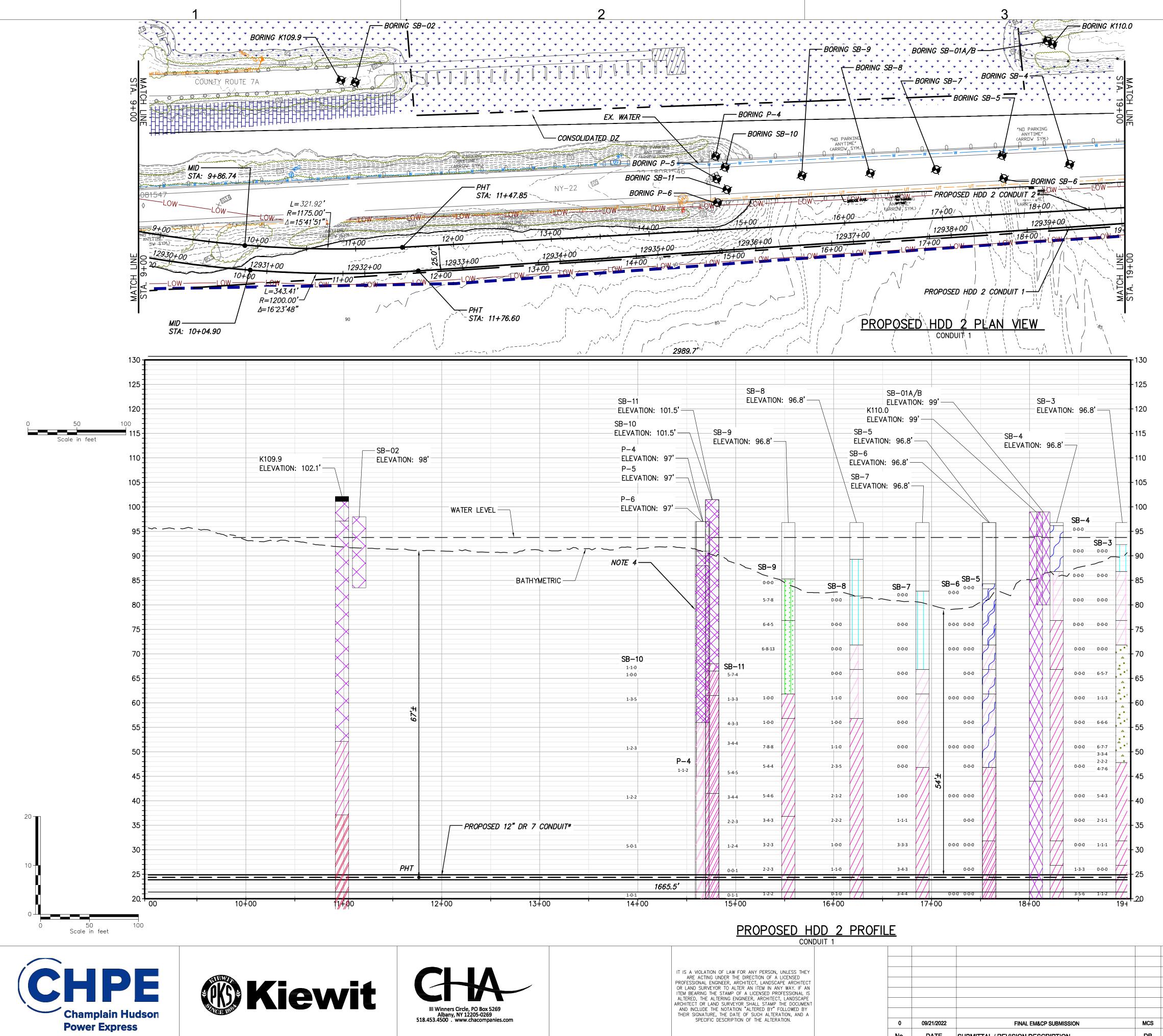
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	00	GP-GM	5	
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Blow Counts per 6" =10-10-10 Recovery %/RQD % =95%/90%



RAWN BY: MCS DESIGNED BY: MB APPROVED BY: JEO REV. NO.

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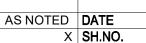
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	ASPHALT Bedrock Boulder CH CH-MH CL CL-ML CONCRETE Fill GC GC-GM GP GP-GC GP-GC GP-GM GW GW-GC GW-GM Limestone MH	Asphalt Bedrock Boulder Fat CLAY SILTY Fat CLAY Lean CLAY Lean CLAY SILTY CLAY Concrete Fill CLAYEY GRAVEL SILTY CLAYEY GRAVEL SILTY CLAYEY GRAVEL SILTY CLAYEY GRAVEL SILTY GRAVEL Poorly Graded GRAVEL Poorly Graded GRAVEL with CLAY Well Graded GRAVEL with CLAY Well Graded GRAVEL with SILT
	Bedrock Boulder CH CH-MH CL CL-ML CENCRETE Fill GC GC-GM GP GP-GC GP-GC GV-GM GW-GC GW-GC GW-GM Limestone	Boulder Fat CLAY SILTY Fat CLAY Lean CLAY SILTY CLAY Concrete Fill CLAYEY GRAVEL SILTY CLAYEY GRAVEL SILTY CLAYEY GRAVEL Poorly Graded GRAVEL Poorly Graded GRAVEL with SILT Well Graded GRAVEL with CLAY Well Graded GRAVEL with SILT
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N N	ML	SILT
	DH	ORGANIC Fat CLAY
	OL	ORGANIC Lean CLAY
i i i	OL/OH	ORGANIC SOIL
	PT	PEAT
— —	Rock	Rock
· · · · · · · · · · · · · · · · · · ·	Sandstone	Sandstone
	SC	CLAYEY SAND
	SC-SM	SILT, CLAYEY SAND
	SHALE	Shale
X	SILTSTONE	Siltstone
	SM	SILTY SAND
	SP	Poorly Graded SAND
· · · · ·	SP-SC	Poorly Graded SAND with CLAY
• • •		Poorly Graded SAND with SILT
		Well graded SAND
		Well Graded SAND with CLAY
		Well Graded SAND with SILT
		Topsoil
		Gravel or Conglomerate 1
		Subgraywacke
1.000		Interbedded Sandstone and Shale
NILLY		Quartzite
		Schist
		Schist
		Gneiss
		Gneiss
		Granite 1
	Void	Void
	Water	Water
· — · · —		Undefined
T	Water Table	Water Table during drilling
\Box	Delayed Water Table	Water Table after drilling
FR F	XPRF.S	KIEWIT PROJECT NO
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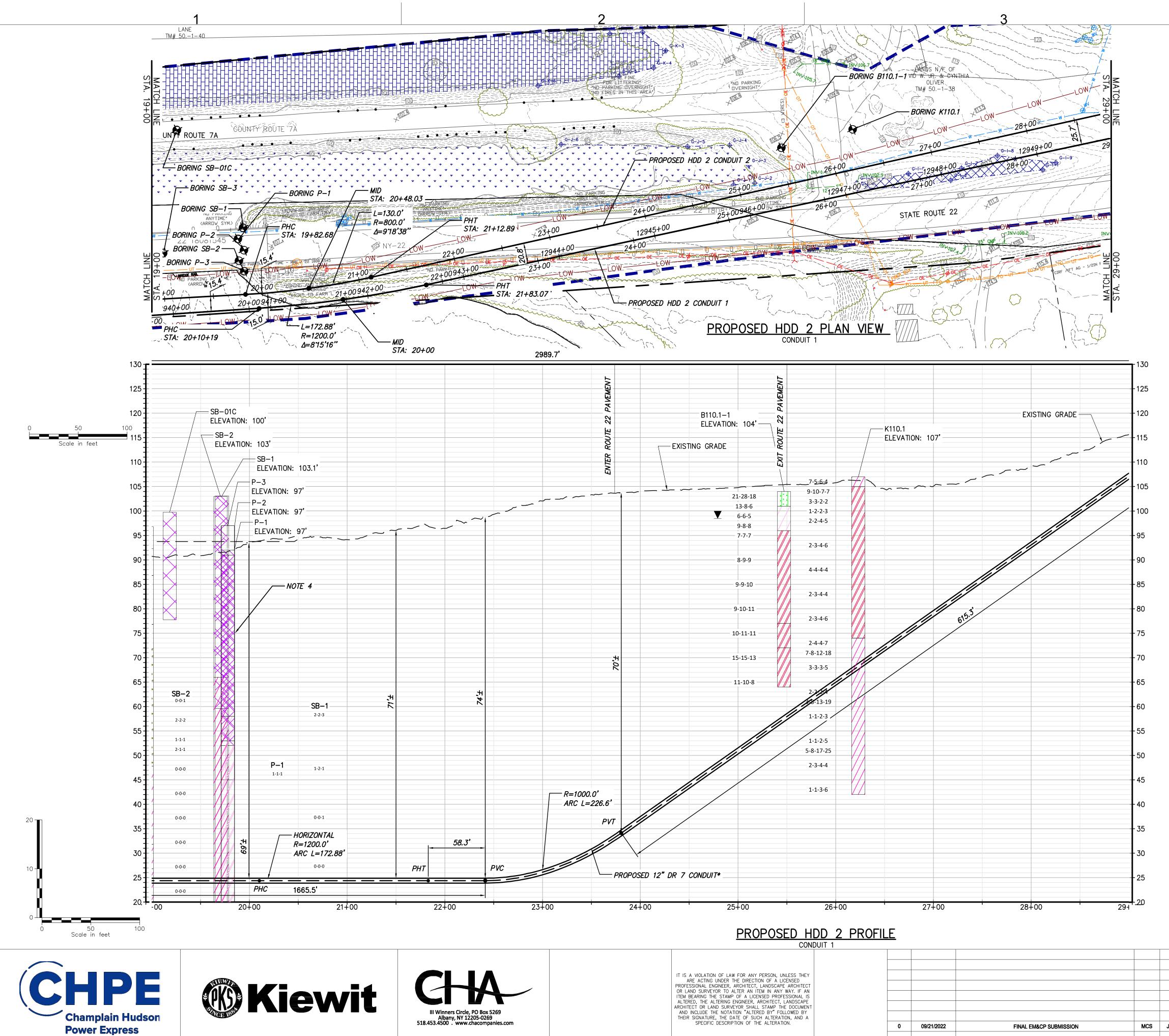
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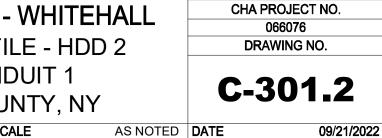


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			Legen	k
		ASPHALT	5	Asphalt
		Bedrock		Bedrock
	· · · •	Boulder		Boulder
		СН		Fat CLAY
		СН-МН		SILTY Fat CLAY
		CL		Lean CLAY
		CL-ML		SILTY CLAY
	/ // /	CONCRETE		Concrete
	\mathbf{X}	Fill		Fill
	5	GC		CLAYEY GRAVEL
		GC-GM	S	ILTY CLAYEY GRAVEL
	56	GM		SILTY GRAVEL
	200	GP	P	oorly Graded GRAVEL
		GP-GC	Poorly	Graded Gravel with CLAY
		GP-GM	Poorly	Graded GRAVEL with SILT
		GW		Well Graded GRAVEL
		GW-GC		Graded GRAVEL with CLAY
		GW-GM		Graded GRAVEL with SILT
		Limestone		Limestone
		MH		Elastic SILT
		ML		SILT
		ОН		DRGANIC Fat CLAY
				DRGANIC Lean CLAY
	55	DL/DH		ORGANIC SOIL
		PT		PEAT
	<u>\ /</u>	Rock		Rock
		Sandstone		Sandstone
		SC		CLAYEY SAND
		SC-SM		SILT, CLAYEY SAND
	· 1. ·	SHALE		Shale
		SILTSTONE		Siltstone
		SM		SILTY SAND
		SP		Poorly Graded SAND y Graded SAND with CLAY
	. /	SP-SC		y Graded SAND with SILT
		SP-SM	FOOR	-
		W2		Well graded SAND
		SW-SC		Graded SAND with CLAY
		SW-SM	Well	Graded SAND with SILT
		Topsoil		Topsoil
		USGS 601	Gro	ivel or Conglomerate 1
		USGS 654		Subgraywacke
		USGS 670	Interbe	dded Sandstone and Shale
		USGS 702		Quartzite
		USGS 705		Schist
		USGS 705		Schist
BORING LOG STRIP LEGEND		USGS 708		Gneiss
B101		USGS 708		Gneiss
$\overline{7}/\overline{7}$	`-``ı	USGS 718		Granite 1
Counts per 6" = 10-10-10		Void		Void
		Water		Water
ery %/RQD % =95%/90% 11000 =UCS		Weathered Rock		Undefined
	T	Water Table		er Table during drilling
	\Box	Delayed Water Table	Wat	er Table after drilling
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				CHA PROJECT NO
	VI _ V		1	000070
SEGMENT 2 - ROUTE 22: DRESDE				066076
CHAMPLAIN HUDSON POWE SEGMENT 2 - ROUTE 22: DRESDEN PROPOSED HDD PLAN AND PRO				DRAWING NO.
SEGMENT 2 - ROUTE 22: DRESDEN PROPOSED HDD PLAN AND PRO	FILE	- HDD 2		DRAWING NO.
SEGMENT 2 - ROUTE 22: DRESDE	FILE NDU	- HDD 2 IIT 1	-	

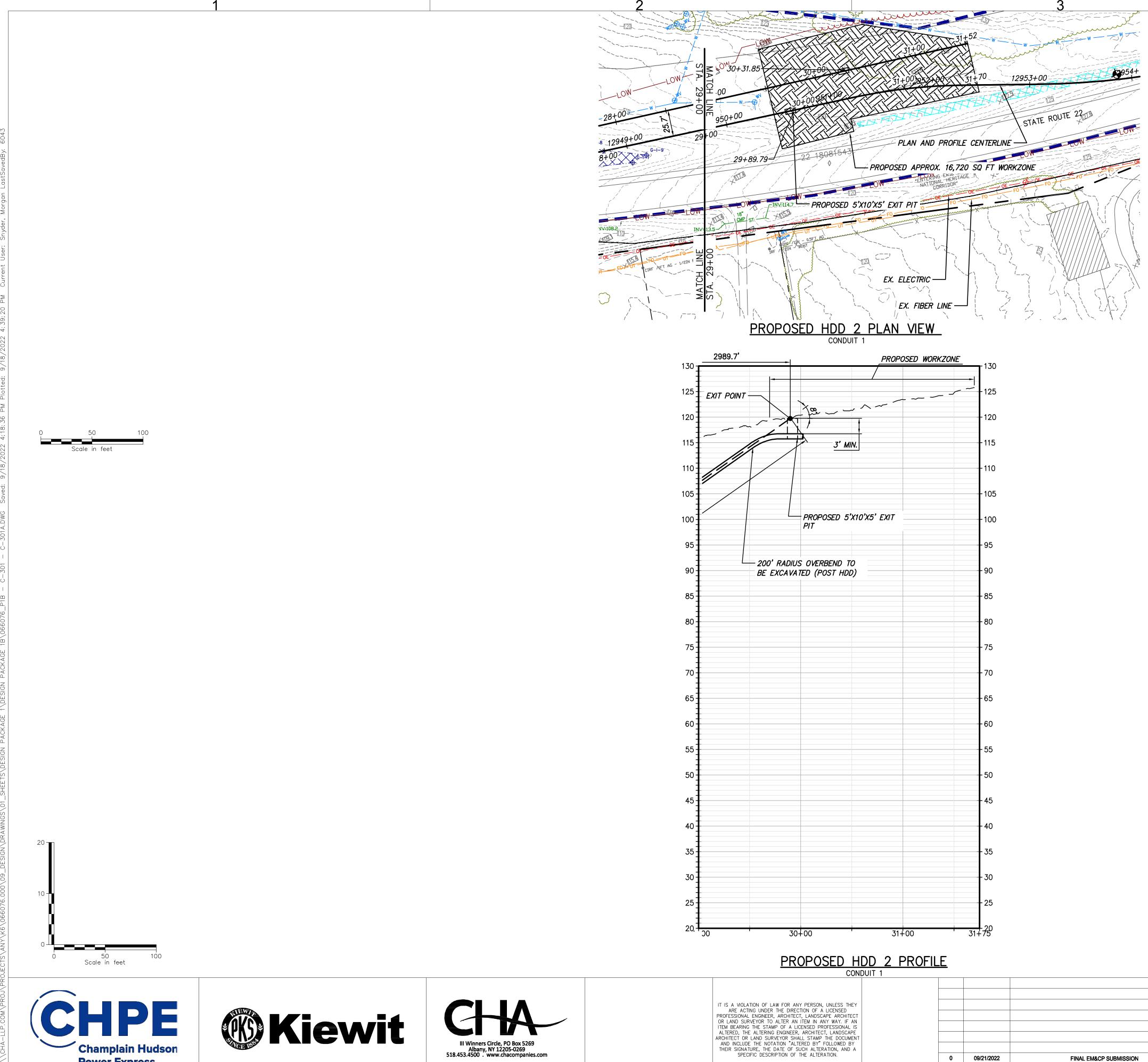


SCALE DRAWN BY: MCS DESIGNED BY: MB APPROVED BY: JEO REV. NO.

X SH.NO.

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MCS JEO

FINAL EM&CP SUBMISSION

DATE SUBMITTAL / REVISION DESCRIPTION

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No.

09/21/2022



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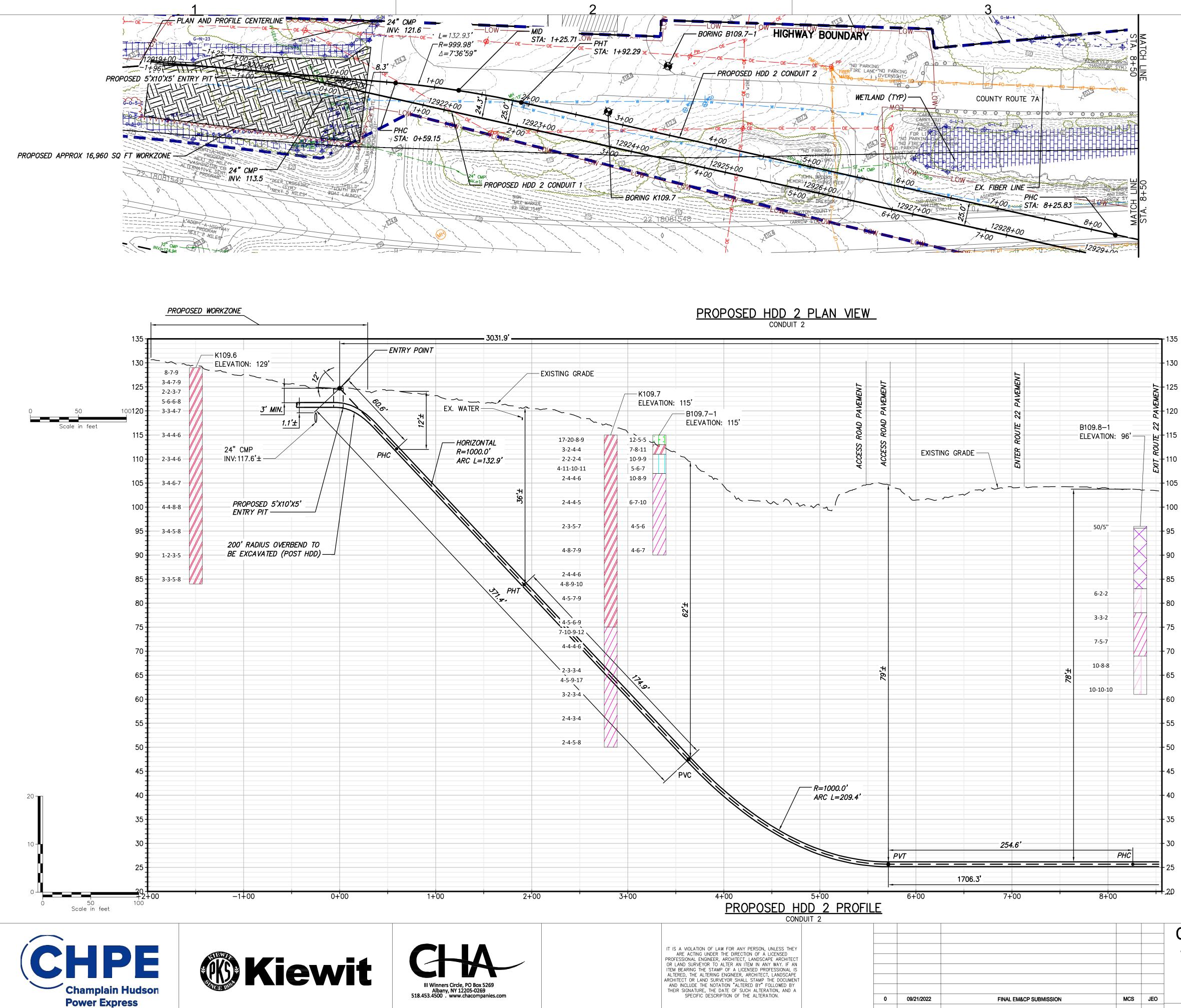
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PROPOSED HDD PLAN AND PRO			. 🖵	066076 DRAWING NO.
CHAMPLAIN HUDSON POW SEGMENT 2 - ROUTE 22: DRESDE				KIEWIT PROJECT N 21162 CHA PROJECT NO
		Delayed Water Table	Wat	er Table after drilling
	T	Water Table		er Table during drilling
very %/RQD % =95%/90% 11000 =UCS	· - · · -	Weathered Rock		Undefined
		Water		Water
Counts per 6" =10-10-10		Void		Vold
$\overline{777}$	[-`]	USGS 718		Granite 1
<u>B101</u>		USGS 708		Gneiss
BORING LOG STRIP LEGEND		USGS 708		Gneiss
		USGS 705		Schist
		USGS 705		Schist
	NITE N	USGS 702		Quartzite
		USGS 670	Interbe	dded Sandstone and Shale
		USGS 654	Tue ± '	Subgraywacke
		USGS 601	երօ	vel or Conglomerate 1
		Topsoil	C	Topsoil
		SW-SM	Well	Graded SAND with SILT
	<u> </u>	SW-SC		Graded SAND with CLAY
		۶W		Well graded SAND
		SP-SM	Poorl	y Graded SAND with SILT
	. /	SP-SC	Poorl	y Graded SAND with CLAY
		SP		Poorly Graded SAND
		SM		SILTY SAND
		SILTSTONE		Siltstone
		SHALE		Shale
		SC-SM		SILT, CLAYEY SAND
	: /: :	SC		CLAYEY SAND
		Sandstone		Sandstone
		Rock		Rock
	<u>« « «</u>	PT		PEAT
	55	 		DRGANIC SOIL
))))			DRGANIC Lean CLAY
		ML DH		SILT DRGANIC Fat CLAY
		MH		Elastic SILT
		Limestone		Limestone
		GW-GM	Well l	Graded GRAVEL with SILT
		GW-GC		Fraded GRAVEL with CLAY
		GW		Well Graded GRAVEL
	jojoj	GP-GM		Graded GRAVEL with SILT
	jojoj	GP-GC	-	Graded Gravel with CLAY
	Ŏ,	GP	Po	oorly Graded GRAVEL
	66	GM		SILTY GRAVEL
	66	GC-GM	S	ILTY CLAYEY GRAVEL
	EXC.	GC		CLAYEY GRAVEL
		Fill		Fill
		CONCRETE		Concrete
		CL CL-ML		Lean CLAY SILTY CLAY
		CH-MH		SILTY Fat CLAY
		СН		Fat CLAY
		Boulder		Boulder
	— — I	Bedrock		Bedrock

SCALE DB APP DRAWN BY: MCS DESIGNED BY: MB APPROVED BY: JEO REV. NO. AS NOTED DATE

X SH.NO.

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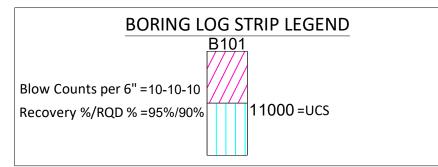
IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED							5
PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR TO ALTER AN ITEM IN ANY WAY. IF AN	_						-
ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE	_						-
AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY	_						-
SPECIFIC DESCRIPTION OF THE ALTERATION, AND A		0	09/21/2022	FINAL EM&CP SUBMISSION	MCS	JEO	-
		No.	DATE	SUBMITTAL / REVISION DESCRIPTION	DB	APP	DRAV
	PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A	ARE ACTING UNDER THE DIRECTION OF À LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A	ARE ACTING UNDER THE DIRECTION OF À LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION OF THE ALTERATION. 0	ARE ACTING UNDER THE DIRECTION OF À LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION OF THE ALTERATION. 0 09/21/2022	ARE ACTING UNDER THE DIRECTION OF À LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION OF THE ALTERATION. 0 09/21/2022 FINAL EM&CP SUBMISSION	ARE ACTING UNDER THE DIRECTION OF À LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION OF THE ALTERATION. 0 09/21/2022 FINAL EM&CP SUBMISSION MCS	ARE ACTING UNDER THE DIRECTION OF À LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION. 0 09/21/2022 FINAL EM&CP SUBMISSION MCS JEO



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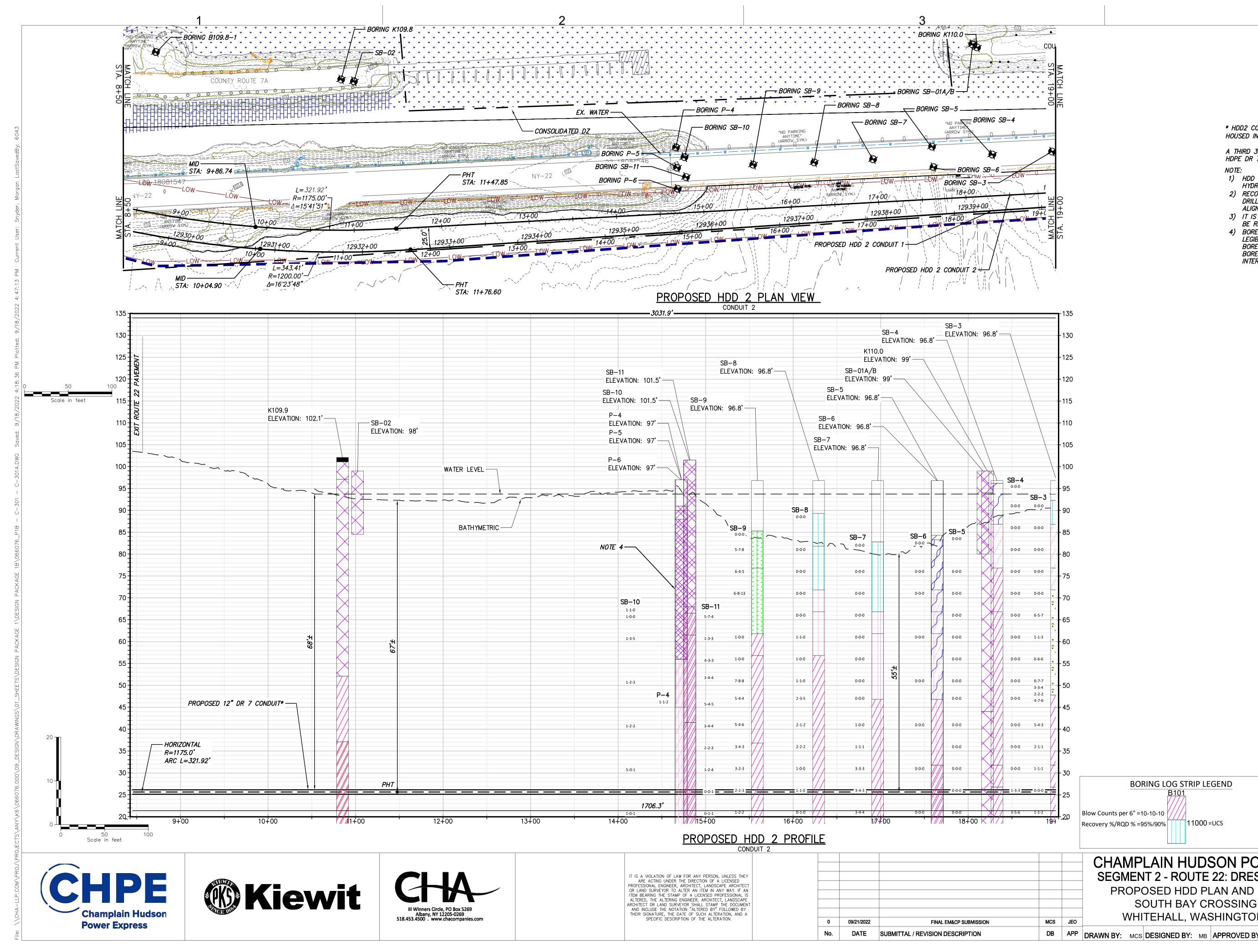


		Legend
	ASPHALT	Asphalt
	Bedrock	Bedrock
• • • • • •	Boulder	Boulder
	СН	Fat CLAY
/////	СН-МН	SILTY Fat CLAY
////	CL	Lean CLAY
	CL-ML	SILTY CLAY
	CONCRETE	Concrete
\mathbf{X}	Fill	Fill
5yrs	GC	CLAYEY GRAVEL
	GC-GM	SILTY CLAYEY GRAVEL
YY	GM	SILTY GRAVEL
	GP	Poorly Graded GRAVEL
<u>N</u>		Poorly Graded Gravel with CLAY
	GP-GC	Poorly Graded GRAVEL with SILT
90	GP-GM	
	GW	Well Graded GRAVEL
	GW-GC	Well Graded GRAVEL with CLAY
	GW-GM	Well Graded GRAVEL with SILT
	Limestone	Limestone
	MH	Elastic SILT
	ML	SILT
	ОН	ORGANIC Fat CLAY
	OL	ORGANIC Lean CLAY
	OL/OH	ORGANIC SOIL
<u> </u>	PT	PEAT
	Rock	Rock
· · · · · · · · · ·	Sandstone	Sandstone
	SC	CLAYEY SAND
	SC-SM	SILT, CLAYEY SAND
	SHALE	Shale
X	SILTSTONE	Siltstone
	SM	SILTY SAND
: : : :	SP	Poorly Graded SAND
	SP-SC	Poorly Graded SAND with CLAY
	SP-SM	Poorly Graded SAND with SILT
	SW	Well graded SAND
	SW-SC	Well Graded SAND with CLAY
	SW-SM	Well Graded SAND with SILT
	Topsoil	Topsoil
/× × \	USGS 601	Gravel or Conglomerate 1
	USGS 654	Subgraywacke
	USGS 670	Interbedded Sandstone and Shale
	USGS 702	Quartzite
7777	USGS 705	Schist
	USGS 705	Schist
((())))) 	USGS 703	Gneiss
	USGS 708	Gneiss
$\langle \dot{\boldsymbol{\zeta}} \rangle \langle $	USGS 708 USGS 718	Granite 1
- 1		
	Void	Vold
	Water	Water
·	Weathered Rock	Undefined
T	Water Table Delayed Water	Water Table during drilling
∇	Table	Water Table after drilling

CHAMPLAIN HUDSON POWER EXPRESS SEGMENT 2 - ROUTE 22: DRESDEN - WHITEHALL PROPOSED HDD PLAN AND PROFILE - HDD 2 SOUTH BAY CROSSING, CONDUIT 2 WHITEHALL, WASHINGTON COUNTY, NY AWN BY: MCS DESIGNED BY: MB APPROVED BY: JEO REV. NO.

21162

CHA PROJECT NO.





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		Legend
	ASPHALT	Asphalt
	Bedrock	Bedrock
· · • 🖓 🖌 · ·	Boulder	Boulder
	СН	Fat CLAY
	СН-МН	SILTY Fat CLAY
	CL	Lean CLAY
	CL-ML	SILTY CLAY
/ /		Concrete
	Fill	Fill
P Y	GC	CLAYEY GRAVEL
$\mathcal{O}\mathcal{O}$	GC-GM	SILTY CLAYEY GRAVEL
	GM	SILTY GRAVEL
	GP	Poorly Graded GRAVEL
	GP-GC	Poorly Graded Gravel with CLAY
	GP-GM	Poorly Graded GRAVEL with SILT
	GW	Well Graded GRAVEL
	GW-GC	Well Graded GRAVEL with CLAY
	GW-GM	Well Graded GRAVEL with SILT
	Limestone	Limestone
↓	МН	Elastic SILT
	ML	SILT
	ОН	ORGANIC Fat CLAY
	OL	ORGANIC Lean CLAY
	OL/OH	ORGANIC SOIL
	PT	PEAT
	Rock	Rock
	Sandstone	Sandstone
	SC	CLAYEY SAND
	SC-SM	SILT, CLAYEY SAND
	SHALE	Shale
\mathbf{X}	SILTSTONE	Siltstone
	SM	SILTY SAND
	SP	Poorly Graded SAND
1 2 2	SP-SC	Poorly Graded SAND with CLAY
	SP-SM	Poorly Graded SAND with SILT
	SW	Well graded SAND
	SM-SC	Well Graded SAND with CLAY
	SW-SM	Well Graded SAND with SILT
	Topsoil	Topsoil
	USGS 601	Gravel or Conglomerate 1
N /	USGS 654	Subgraywacke
	USGS 670	Interbedded Sandstone and Shale
	USGS 670 USGS 702	Interbedded Sandstone and Shale Quartzite
	USGS 702	Quartzite
	USGS 702 USGS 705	Quartzite Schist
	USGS 702 USGS 705 USGS 705	Quartzite Schist Schist
	USGS 702 USGS 705 USGS 705 USGS 708	Quartzite Schist Schist Gneiss
	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708	Quartzite Schist Schist Gneiss Gneiss
	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 718	Quartzite Schist Schist Gneiss Gneiss Granite 1
	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 718 Void	Quartzite Schist Schist Gneiss Gneiss Granite 1 Void
	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 718 Void Water	Quartzite Schist Schist Gneiss Gneiss Granite 1 Void Water
	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 718 Void Water Weathered Rock	Quartzite Schist Schist Gneiss Gneiss Granite 1 Void Water Undefined
	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 718 Void Water	Quartzite Schist Schist Gneiss Gneiss Granite 1 Void Water Undefined Water Table during drilling
	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 718 Void Water Weathered Rock Water Table	Quartzite Schist Schist Gneiss Gneiss Granite 1 Void Water Undefined
\Box	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 718 Void Water Weathered Rock Water Table Delayed Water Table	Quartzite Schist Schist Gneiss Granite 1 Void Water Undefined Water Table during drilling Water Table after drilling
WER E	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 718 Void Water Weathered Rock Water Table Delayed Water Table	Quartzite Quartzite Schist Schist Gneiss Gneiss Granite 1 Void Water Undefined Water Table during drilling Water Table after drilling KIEWIT PROJECT NO 21162
WER E	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 718 Void Water Weathered Rock Water Table Delayed Water Table	Quartzite Quartzite Schist Schist Gneiss Gneiss Granite 1 Void Void Vater Undefined Water Table during drilling Water Table after drilling KIEWIT PROJECT NO SS (CHA PROJECT NO.
WER E DEN - W	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 718 Void Water Weathered Rock Water Table Delayed Water Table EXPRES	Quartzite Quartzite Schist Schist Greiss Greiss Granite 1 Void Vater Undefined Water Table during drilling Water Table after drilling KIEWIT PROJECT NO O66076
WER E DEN - W PROFILE	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 708 USGS 718 Void Water Weathered Rock Water Table Delayed Water Table EXPRES /HITEHAL	Quartzite Quartzite Schist Schist Gneiss Gneiss Granite 1 Void Void Vater Undefined Water Table during drilling Water Table after drilling KIEWIT PROJECT NO SS (CHA PROJECT NO.
WER E DEN - W PROFILE	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 708 USGS 718 Void Water Weathered Rock Water Table Delayed Water Table EXPRES /HITEHAL	Quartzite Quartzite Schist Schist Greiss Greiss Granite 1 Void Void Vater Undefined Water Table during drilling Water Table after drilling KIEWIT PROJECT NO. 066076 DRAWING NO.
WER E DEN - W	USGS 702 USGS 705 USGS 705 USGS 708 USGS 708 USGS 708 USGS 718 Void Water Weathered Rock Water Table Delayed Water Table EXPRES /HITEHAL - HDD 2 IT 2	Quartzite Quartzite Schist Schist Greiss Greiss Granite 1 Void Vater Undefined Water Table during drilling Water Table after drilling KIEWIT PROJECT NO 21162 CHA PROJECT NO. 066076

SEGMENT 2 - ROUTE 22: DRES PROPOSED HDD PLAN AND

BORING LOG STRIP LEGEND

SOUTH BAY CROSSING WHITEHALL, WASHINGTO

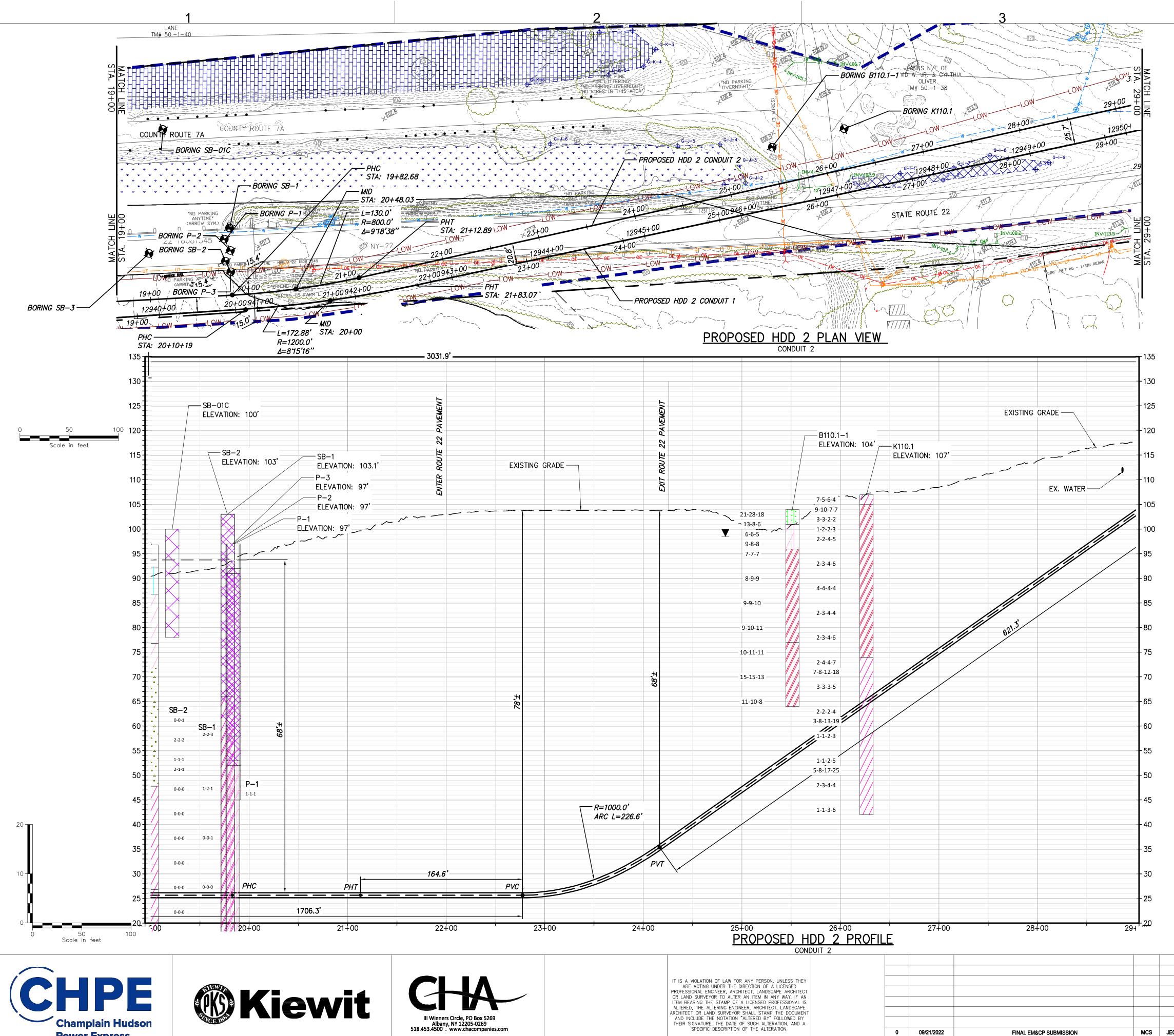
SCALE DB APP DRAWN BY: MCS DESIGNED BY: MB APPROVED BY: JEO REV. NO.

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09/21/2022

XXX OF XXX



Power Express

MCS JEO

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No.

09/21/2022

FINAL EM&CP SUBMISSION

DATE SUBMITTAL / REVISION DESCRIPTION



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			Legend
		ASPHALT	Asphalt
		Bedrock	Bedrock
	\ 	Boulder	Boulder
		СН	Fat CLAY
		CH-MH	SILTY Fat CLAY
	////	CL	Lean CLAY
		CL-ML	SILTY CLAY
		CONCRETE	Concrete
		Fill	Fill
	55	GC	CLAYEY GRAVEL
	00	GC-GM	SILTY CLAYEY GRAVEL
	56	GM	SILTY GRAVEL
	50	GP	Poorly Graded GRAVEL
	00	GP-GC	Poorly Graded Gravel with CLAY
	66	GP-GM	Poorly Graded GRAVEL with SIL
		GW	Well Graded GRAVEL
		GW-GC	Well Graded GRAVEL with CLAY
	65	GW-GM	Well Graded GRAVEL with SILT
		Limestone	Limestone
		МН	Elastic SILT
		ML	SILT
		ΠH	ORGANIC Fat CLAY
	<u> </u>	OL	ORGANIC Lean CLAY
	55	OL/OH	ORGANIC SOIL
	<u>n n n</u>	PT	PEAT
		Rock	Rock
		Sandstone	Sandstone
	• •/•	SC	CLAYEY SAND
		SC-SM	SILT, CLAYEY SAND
	- 71	SHALE	Shale
		SILTSTONE	Siltstone
		SM	SILTY SAND
		SP	Poorly Graded SAND
		SP-SC	Poorly Graded SAND with CLAY
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		SW-SM	Well Graded SAND with SILT
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		USGS 670	Interbedded Sandstone and Shal
		USGS 702	Quartzite
	111.1	USGS 702	Schist
		USGS 705	Schist
		USGS 703	Gneiss
BORING LOG STRIP LEGEND		USGS 708	Gneiss
<u>B101</u>	<u> </u>		
$\langle /// \rangle$		USGS 718 Void	Granite 1 Void
Counts per 6" =10-10-10			
very %/RQD % =95%/90%		Water	Vater
		Weathered Rock	Undefined
		Water Table Delayed Water	Water Table during drilling
;	\Box	Table	Water Table after drilling
		VDDEC	KIEWIT PROJECT N
CHAMPLAIN HUDSON POV SEGMENT 2 - ROUTE 22: DRESE			CHA PROJECT NO
			000076
PROPOSED HDD PLAN AND P	KOHILE	- HUU 2	DRAWING NO.
SOUTH BAY CROSSING, (C-301A
WHITEHALL, WASHINGTON	COUNT	Y. NY	

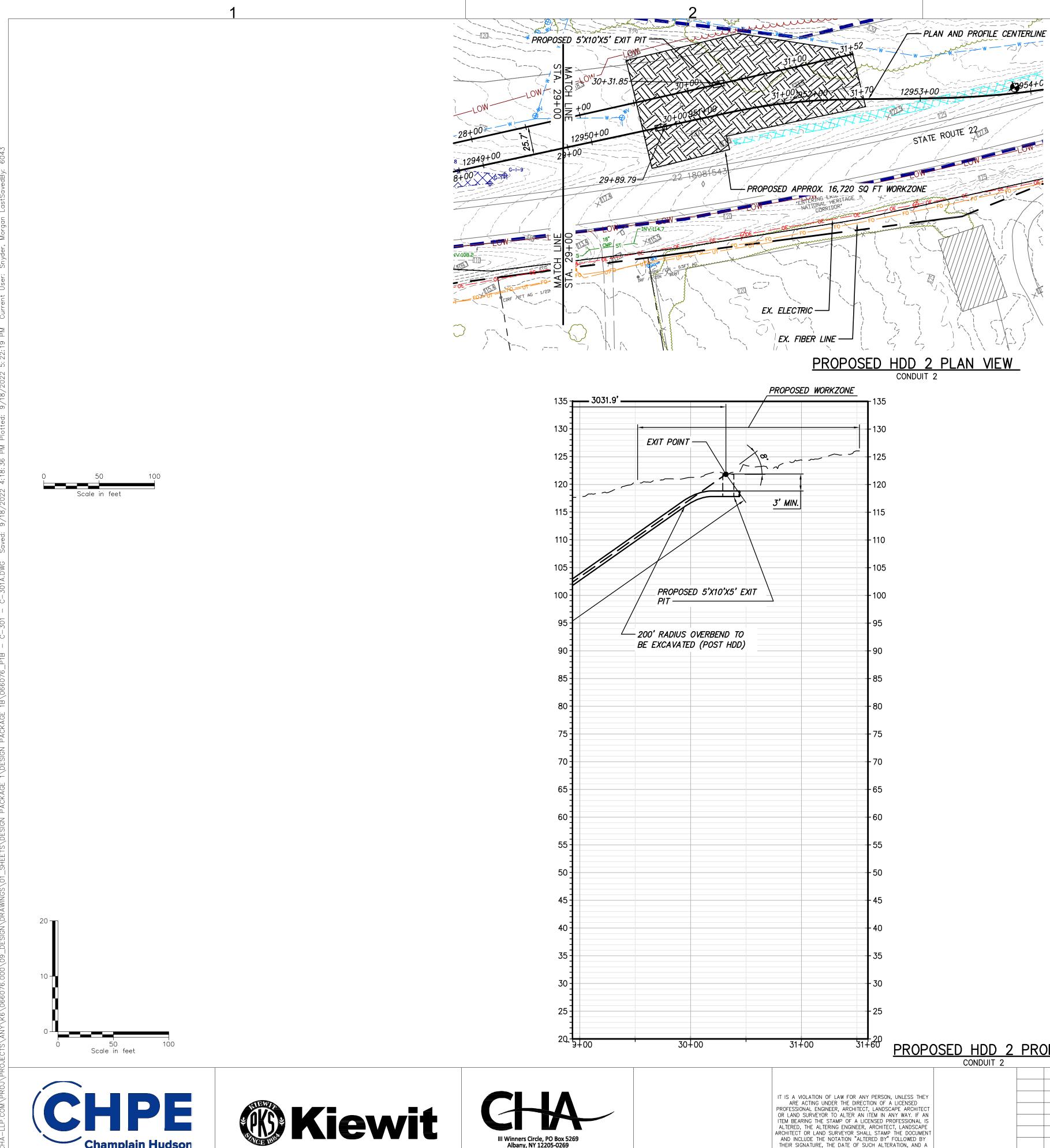
SCALE DB APP DRAWN BY: MCS DESIGNED BY: MB APPROVED BY: JEO REV. NO.

Blow Counts per 6" =10-10-10

Recovery %/RQD % =95%/90%

09/21/2022

XXX OF XXX



III Winners Circle, PO Box 5269 Albany, NY 12205-0269 518.453.4500 . www.chacompanies.com

Champlain Hudson

Power Express

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	No.	DATE	SUBMITTAL / REVISION DESCRIPTION	DB	APP	DR/





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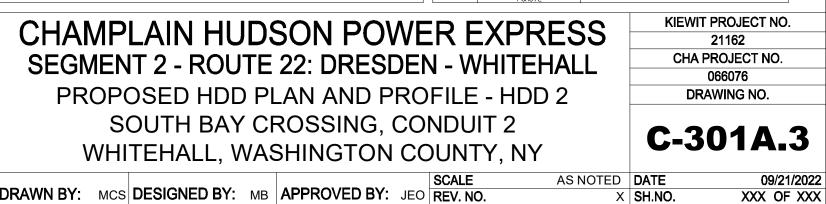
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	- HDD 2	DRAWING NO.
		066076
1 - N	/HITEHAL	
K E	EXPRES	SS 21162
		KIEWIT PROJECT I
∇	Delayed Water Table	Water Table after drilling
T	Water Table	Water Table during drilling
· · · · · · · ·	Weathered Rock	Undefined
	Water	Water
	Void	Void
- 1	USGS 718	Granite 1
<u>K ((</u>	USGS 708	Gneiss
	USGS 708	Gneiss
	USGS 705	Schist
	USGS 705	Schist
	USGS 702	Quartzite
	USGS 670	Interbedded Sandstone and Sho
	USGS 654	Subgraywacke
<u> </u>	USGS 601	Gravel or Conglomerate 1
₩XX	Topsoil	Topsoil
	SW-SM	Well Graded SAND with SILT
<u>^</u>	SW-SC	Well Graded SAND with CLAY
	SM.	Well graded SAND
	SP-SM	Poorly Graded SAND with SILT
	SP-SC	Poorly Graded SAND with CLAY
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	SILTSTONE	Siltstone
	SHALE	Shale
. /. •	SC-SM	SILT, CLAYEY SAND
	20	CLAYEY SAND
/		
	Sandstone	Sandstone
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55	DL/DH	DRGANIC LEAN CLAY
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	ML	SILT
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	Limestone	Limestone
MA	GW-GM	Well Graded GRAVEL with SILT
	GW-GC	Well Graded GRAVEL with CLAY
	GW	Well Graded GRAVEL
RANK	GP-GM	Poorly Graded GRAVEL with SIL
200	GP-GC	Poorly Graded Gravel with CLA
200	GP	Poorly Graded GRAVEL
M M M	GM	SILTY GRAVEL
	GC-GM	SILTY CLAYEY GRAVEL
P-Y-3	GC	CLAYEY GRAVEL
	Fill	Fill
	CONCRETE	Concrete
	CL CL-ML	Lean CLAY SILTY CLAY
[//]	СН-МН	SILTY Fat CLAY
	СН	Fat CLAY
· · ·	Boulder	Boulder
· · 🖉 · ·	Bedrock	
⊢ −	Dooloocly	Bedrock

Recovery %/RQD % =95%/90%

Blow Counts per 6" =10-10-10

BORING LOG STRIP LEGEND



B



Inadvertent Release Contingency Plan For Horizontal Directional Drilling in Segments 1 & 2 – Packages 1A & 1B

Putnam to Whitehall Washington County, New York

CHA Project Number: 066076

Prepared for: Transmission Developers Inc. 1301 Avenue of the Americas, 26th Floor New York, NY 10019



Prepared by: CHA Consulting, Inc. III Winners Circle Albany, New York 12205 (518) 453-4500

9/18/2022

September 2022

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2.0	DESCRIPTION OF THE HDD PROCESS	3
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1.0 INTRODUCTION

CHA Consulting, Inc. (CHA) and the Kiewit Team, with the support of Boscardin Consulting Engineers (BCE), proposes to design and construct approximately 170 horizontal directional drilling (HDD) crossings for a pair of HVDC electrical transmission cables plus a telecommunications line located in upland areas of the Hudson River Valley of New York for Segments 1 through 7 from Putnam Station to Schenectady, NY. Horizontal directional drilling (HDD) methods will be used to route the crossings below congested areas, railroads, under/around obstructions (e.g., existing infrastructure or utilities), and below wetlands and bodies of water. The portions of the cable between HDD bores will be installed in PVC conduits via trenching methods. The trenching construction is addressed in a separate report.

The underground construction of the two HVDC electrical transmission cables is proposed to be housed in individual 10-inch-diameter DR 9 HDPE conduits spaced a distance dependent on depth and soil Thermal Resistivity (TR) values provided by NKT and as shown on drawings plans. A third, typically 2-inch-diameter DR 9 conduit will be bundled with one of the 10-inch-diameter conduits for a telecommunications line. The conduits are to be installed in 16-inch to 22-inch final reamed diameter bore holes. Final conduit diameter and DR values will depend on length and depth of the HDD bores. Longer and deeper bores may require a larger diameter (i.e. 12-inch and 3 inch) and larger DR values (i.e. DR 7) to resist tension stresses during installation and collapsing long-term. This is checked and determined on a case-by-case basis and design sizes are shown on the design drawings.

This Inadvertent Release Contingency Plan (IRCP) is for Segments 1 & 2 – Packages 1A & Package 1B which includes three HDD crossings: HDD #1 crossing Mill Brook culverts and under Lake Road; and HDD #2 crossing under South Bay adjacent to State Route 22.

HDD is a widely used trenchless construction method to install conduits with limited disturbance to the ground around the bore alignment and minimal ground surface impacts above the alignment. The goal for using HDD methods is to install the conduits while controlling and minimizing the amount of impact on water bodies, congested areas, existing underground obstructions, and to the wetlands, to the extent possible. A primary potential environmental concern associated with HDD involves the inadvertent release of drilling fluids, also referred to as drilling mud, during the drilling process, which is addressed in this plan. The purpose of this plan is to establish general procedures to prevent a fluid release (sometimes referred to as a frac-out) during HDD construction and to present steps to manage, control and minimize the impacts in the event that an inadvertent release of drilling fluid occurs. The objectives of this plan are to:

- Provide an overview of the HDD process with a specific focus on the composition, management and use of drilling fluids;
- Identify controls to be implemented during construction to minimize the potential of an inadvertent release;
- Identify the planned means of monitoring to permit early detection of inadvertent releases;
- Identify planned means to protect areas that are considered environmentally sensitive (rivers, wetlands, other biological resources or cultural resources);
- Establish site-specific environmental protection measures to be utilized prior to, during, and following drilling and conduit installation activities to minimize and control erosion and sediment releases to adjoining wetlands or watercourses;
- Have site specific preplanned general response programs in place at the start of construction that is understood and can be implemented immediately by all field crews in the event of an inadvertent release of drilling fluid occurs; and
- Establish a chain of command for reporting and notifying, in a timely manner, the construction management team, the Certificate Holders, and the proper authorities in the event of an inadvertent release of drilling fluid and of the preplanned actions that are to be implemented.

It is important to note that the plan in this document serves as the guiding framework for confirming that the HDD Construction Subcontractor (HDD Subcontractor) is adhering to the specifications and provisions to be protective of the environment. Since there are a variety of potential measures listed in this document available for preventing inadvertent releases and mitigating the effects of a release should one occur. The specifications require that each HDD Subcontractor submit to the project design team, for its review and acceptance, a supplemental site and HDD Subcontractor specific means and methods plan for each HDD crossing reaffirming and detailing how the HDD Subcontractor will conform with the requirements of this plan and the project specifications to prevent inadvertent releases and to mitigate any effects of a release

should one occur. The supplemental plan by the HDD Subcontractor shall be consistent with the site conditions and constraints, and the HDD Subcontractor's selected means, methods and equipment. The selected HDD Subcontractor will be responsible for incorporating specific permit conditions, applicable regulatory requirements, site specific environmental features, and geotechnical information not available at this time into its submittal. The submittal shall be reviewed and approved by the design team and the Environmental Inspector prior to the start of construction of a specific HDD location.

2.0 DESCRIPTION OF THE HDD PROCESS

The Horizontal Directional Drilling process begins by mechanically excavating shallow (approximately 5 feet wide by 10 feet long by 4 to 5 feet deep entry and exit pits at either end of the directional bore alignment within a designated work area. Typical work areas and equipment layouts are discussed in Design Summary Report. However, final individual work areas and equipment layouts will be site specific and depend on the length of bore, size of drill rig to be used, and site constraints. A small diameter (on the order of 5 to 9 inches in diameter) pilot bore is then drilled from the entry pit using directional boring methods. During the pilot bore, a drilling fluid (typically bentonite and water based with selected NSF certified additives) to improve and modify fluid stability, carrying capacity, and drilling properties to address site-specific ground characteristics and HDD Subcontractor preferences is pumped through nozzles in the drill head to support the hole and to hydraulically transport drill cuttings from the drill bit back to the entry pit. Environmentally acceptable, NSF (formerly National Sanitation Foundation) certified, additives are required by specification for use on this project and those planned for use by the HDD Subcontractor will be checked for compliance by the design team prior to their use.

A guidance system is mounted immediately behind the drilling head to allow the crew to track and steer the path of the drilling so that it follows the preplanned alignment within the specification's permitted tolerances. The drilling fluid holds the cuttings in suspension and carries the drill cuttings back through the annular space between the drill rods and the bore hole wall to the entry pit where it is collected and processed for re-used by a recycling system. The cuttings are separated from the bentonite, using screens, centrifuges, and desanding units which prepares the bentonite for re-use. Once the pilot bore reaches the exit pit, a larger diameter back-reaming head is

then attached to the drill string and pulled back through the pilot hole to enlarge the hole. Depending on the size of the conduit to be installed and the ground conditions, several successively larger reaming passes may be needed. Again, a bentonite and water slurry is pumped into the bore hole during reaming to remove cuttings and to stabilize the bore hole. Lastly, the drill string is pulled back through the bore hole with the new, preassembled conduit attached to it in one continuous process until the lead end of the conduit emerges at the entry pit. Final reaming or swabbing and conduit pull back may be combined.

Specific to this plan, it is important to have an awareness of the function and composition of the HDD drilling fluids. The drilling fluid composition and drilling fluid management are integral components of the HDD process with the following primary purposes:

- Support and stabilize the drill hole,
- Suspend and transport the cuttings from drill bit through the drill hole annulus,
- Control fluid loss through the bore's side walls by forming a filter cake on the bore hole walls,
- Managing and modifying the drilling fluid mix to improve its cutting carrying characteristics, its pumpability, and its hole stabilization and support characteristics,
- Power the downhole cutting tools (e.g., via mud motors if required); and,
- Serve as a coolant and lubricant to the drill bit during the drilling process and serve as a lubricant during the conduit insertion process.

The drilling fluids are composed primarily of potable water, which will likely be obtained from nearby sources selected and permitted by the HDD Subcontractor. As mentioned above, the drilling fluid also contains bentonite clay as a viscosifier. Bentonite is a naturally occurring, nontoxic, inert substance that meets NSF/ANSI 60 NSF Drinking Water Additives Standards and is frequently used for drilling potable water wells. While bentonite is non-toxic and commonly used in farming practices, it has the potential to impact plants, fish and their eggs if discharged to waterways in significant quantities. Frequently, additives are used to: amend the drilling fluid, improve its compatibility with the ground and groundwater chemical characteristics, improve its cutting suspension and carrying characteristics. Environmentally acceptable (i.e. NSF certified) additives are required by specification for this project and before the start of work at a specific HDD, the HDD Subcontractor is required to submit crossing data environmental and toxicity data

including Safety Data Sheets (SDSs) for review and acceptance by the design team regarding any additives to be used.

During the HDD process and subsequent conduit insertion, the drilling fluid pumped downhole will tend to flow along the path of least resistance. Generally, this will be though the annulus between the drill string and the drill hole side wall. However, the bore alignment may encounter ground conditions where the path of least resistance is an existing fracture, fissure, hole of anthropogenic origin, areas with low overburden confinement, areas of hole collapse, or coarse gravel zones in the soil or rock substrate. When this occurs, circulation can be lost or reduced. This is a common occurrence in the HDD process but does not necessarily prevent completion of the bore or result in a release to the environment. However, the environment may be impacted if the fluid inadvertently releases to the surface at a location on a waterway's banks or within a waterway or wetland. Again, additives to amend the properties of the drilling fluid may be used as necessary to prevent and limit releases and losses through such paths of lower flow resistance.

3.0 ORGANIZATION AND STAFFING RESPONSIBILITIES

The organizational chart shown below lists the contact information of the principal organizations involved in this project. The remainder of Section 3 discusses the roles and responsibilities of these principal organizations.

Organizational Chart

Entity	Contact Information
	Name, Title
Certificate Holders	Phone
	Email
Construction Manager	TBD
HDD Design/Engineer Team	TBD
HDD Construction	TBD
Subcontractor	
Environmental Inspector	r TBD
U.S. Army Corps of Engineers, New York District Office	USACE New York District Upstate Regulatory Field Office ATTN; CENAN-OP-UR, Bldg. 10, 3 rd Floor North 1 Buffington Street Watervliet, NY 12189-4000 518-266-6350 <u>cenan.rfo@usace.army.mil</u>
New York State Department of Public Service	Matthew Smith Department of Public Service Empire State Plz 3 Albany, NY 12223 (518) 402-5141 matthew.smith@dps.ny.gov
New York State Department of Environmental Conservation	Regional Office(s) Information NYSDEC REGION 5 Sub-Office Regional Permit Administrator 232 Golf Course Rd Warrensburg, NY 12885-1172 518-623-1281 dep.r5@dec.ny.gov
New York State Department of Environmental Conservation (Spills)	NYS Spill Hotline: 1-800-457-7362

3.1 **RESPONSIBILITIES OF VARIOUS ORGANIZATIONS**

The principal organizations involved in this project include the Regulatory Agencies, Certificate Holders, Design Engineer, HDD Construction Subcontractor, Construction Manager, and Environmental Inspector. The roles and responsibilities of the principal organizations are discussed in the following subsections and are shown in the organizational chart included above.

3.2 REGULATORY AGENCIES

The Certificate of Conditions issued by the NY Public Service Commission is the primary regulatory agency for the requirements associated with the project. The Champlain Hudson Power Express (CHPE) Route Project also has permits from the Department of Energy, and the US Army Corps of Engineers, and the New York Water Quality Certification. Various HDDs within this package take place within or adjacent to wetlands, underneath or adjacent to bodies of water, and underneath or adjacent to DOT roads. Measures are discussed throughout this report to control/mitigate any potential releases before environmentally sensitive boundaries are reached or impacted.

3.3 CERTIFICATE HOLDERS

The project Certificate Holders are TDI. TDI's Project Manager will have the overall responsibility to coordinate this project for TDI. The Project Manager, will be responsible for correspondence and coordination among all parties and will have the authority to stop work as necessary.

3.4 DESIGN ENGINEER

The FEED Design Engineer for the HDD Design is CHA and Kiewit in collaboration with BCE. During construction, the yet to be confirmed Design Engineer during construction will be responsible for reviewing and approving required Subcontractor submittals, shop drawings, and material certificates. Power Engineers will also take responsibility for review and acceptance of submittals, and documenting the materials and methods used in performance of the construction work to document that the construction complies with the contract documents.

3.5 THIRD-PARTY ENGINEER

The Third-Party Engineer for the HDD inadvertent return analysis has yet to be confirmed. During construction, the chosen Third-Party Engineer will be assisting Transmission Developers Inc. with the review of the Subcontractors Inadvertent Release Plan and providing technical assistance as needed with the HDD installation.

3.6 CONSTRUCTION MANAGER

The Construction Manager for this project has yet to be selected. The Construction Manager will be responsible for on-site management of the project for the Certificate Holders to ensure overall Subcontractor compliance with the EM&CP documents, environmental permits, and, local and federal regulations.

3.7 HDD CONSTRUCTION SUBCONTRACTOR

The HDD Subcontractors for the various HDD crossings of this project have yet to be selected. The Subcontractor will be responsible for completion of the conduit installation by HDD methods in accordance with the design criteria, contract documents, environmental compliance permits and federal regulations. The Subcontractor will be expected to use the appropriate construction procedures and techniques to complete the project, including supplemental site specific and means and methods specific HDD Subcontractor-prepared Inadvertent Release Prevention and Contingency Plans reviewed and accepted by the design team for each crossing in accordance with the contract documents.

The HDD Drill Operator (Drill Operator) will be responsible for operating the HDD drill rig, and observing and managing changes in annular fluid pressure or loss of circulation. The Drill Operator will communicate with other members of the drill crew as needed when issues arise. The Subcontractor will be responsible for developing the specific lines of communication within their organization and shall dedicate a responsible person(s) for monitoring and communicating inadvertent releases to the Construction Management team and Environmental Inspector.

3.8 Environmental Inspector

The Environmental Inspector for this project has not yet been determined. In general, the Environmental Inspector will perform full-time observation and documentation during the HDD activities at a specific site. The Environmental Inspector will be responsible for coordination with all county, state and federal resource agencies, compliance with and changes to any environmental permits.

The Environmental Inspector shall have the authority to stop work when the environmental permit conditions are not being followed or when appropriate environmental precautions are being disregarded by the HDD Subcontractor.

3.9 LINES OF COMMUNICATION AND AUTHORITY

Formal lines of communication will generally follow the established lines of authority. However, open communications between all parties will be encouraged to facilitate more efficient communication and coordination.

3.10 TRAINING

The HDD Subcontractor will verify and document that all construction personnel have appropriate environmental training before they begin work. The Environmental Inspector will also conduct a project orientation meeting for staff assigned with specific roles during the HDD installation and will review the site-specific environmental concerns and permit conditions. The Certificate Holders and Design Engineer will also attend the orientation meeting to review the procedures that will be used to document inadvertent releases in accordance with the HDD specifications.

4.0 FLUID RELEASE MINIMIZATION MEASURES

4.1 GEOTECHNICAL INVESTIGATION

The first steps taken to minimize the potential risk of an inadvertent release included conducting a geotechnical investigation at the site to develop an understanding of the ground around the planned HDD bores. Test borings were conducted near the proposed cable alignment within or immediately adjacent to the HDD sites. CHA understand that each boring has been backfilled and sealed with a cement or cement/bentonite grout to limit the risk of a release through an abandoned bore hole during the HDD construction.

4.2 HDD DESIGN

The HDD crossing is being designed to reduce the potential risk of an inadvertent fluid release during construction. General design considerations for HDD include:

- Depth of cover during profile design (based on test borings) to limit the potential inadvertent break through to the water body, road, wetlands, or ground surface;
- Typically, potential exists for releases near the entry and exit pits of a bore. The distance where there is a potential for releases at the ends depends on the soil conditions, the slope of the ground surface and the length of the bore. Generally, the longer and deeper the bore the greater the slurry pressures required to hold the borehole open and to carry the cuttings back to the entry or exit pit;
- Specific provisions regarding design for underwater cable installation (i.e. via the use of temporary dredged cofferdams or steel conduit riser pipes for pressure relief);
- Generally, for the formation of inadvertent releases, the more critical stage of the HDD process tends to be during the initial pilot hole drilling when the annular space between the bore sidewall and the drill string is the smallest and therefore requires large slurry pressures to overcome flow resistance to carry cuttings back to the entry pit;
- Adjusting the drill alignment to miss existing infrastructure including existing utilities, pile foundations, and other obstacles;
- Establishing a drill alignment line that allows for gradual angular changes to minimize pressure build-up and limit pull back stresses and bending stresses in

the conduit, as well as being compatible with the bending capacity of the drill steel;

- Requiring drilling fluid composition, flow rates, and drilling procedures that minimize drilling fluid pressures;
- Requiring drilling fluids that adequately address site-specific drilling concerns while posing the least threat to the environment;
- Requiring monitoring and controlling drilling fluid pressures with down-the-hole sensors during pilot hold drilling; and
- Requiring that, during the performance of any HDD waterbody crossing, contractors monitor the use of NSF certified drilling solution (Article VII: General Condition No. 114 [m]) and, in the event of a detected release of fluid, implement the procedures specified in the approved EM&CP. For any release occurring in a waterbody, the Certificate Holders shall immediately notify DPS Staff and NYSDEC Region 5 Staff of details of the release and the course of action they recommend taking.

4.3 CONTINGENCY PLAN

As mentioned above, prior to construction the selected HDD Subcontractor will be required to submit a supplemental site-and Subcontractor-Specific Inadvertent Release Contingency Plan for review and approval by design team. The project specifications require that the following major elements be addressed in detail in the Subcontractor's Plan:

- Work plan and detailed description of the drilling program (details for executing pilot hole, reaming, pull-back operations, and schedule), this plan shall include necessary procedures for addressing problems that are typically encountered during HDD installations through the anticipated subsurface for each drill location and to prevent inadvertent releases of drilling slurry;
- Drilling fluid composition design and on-hand amendments to alter fluid properties to reduce pressures, potential for plugging, and seepage losses;
- Description of the planned drilling equipment and drill site layout;
- SDS information for all drilling fluid products proposed for use;
- Procedures for drilling fluid pressure control, and fluid and pressure loss monitoring and management to aid in the detection of an inadvertent release (i.e., metering of makeup water, recording of drilling fluid product quantities utilized, fluid return

volumes, fluid and cuttings disposal quantities, turbidity of river water, etc.);

- Contingency plans for addressing inadvertent releases into wetlands, or other sensitive areas, which includes the specific procedures used to halt the release and then contain, clean-up, and remove materials from the release site;
- Notification procedures and chain-of-command in the event of a release;
- Criteria for evaluating the need for a drill hole abandonment and the associated plan for sealing the drill hole if abandoned;
- Drilling fluid management and disposal procedures;
- The work plan and detailed drilling program description should include documentation regarding site restoration, vegetation management, sedimentation and erosion control, and hazardous material usage (if applicable). The intended approach will be in compliance with those measures presented in the Project EM&CP.
- Notice shall be provided to residents, businesses, and building, structure, and facility (including underground, aboveground and underwater facilities) owners and operators within one hundred (100) feet of any HDD staging area or trenching activity with an offer to inspect foundations before, during, and after construction. Additional detail regarding this notice, associated inspections, intended benefits, proof of notice, cost reimbursements and associated construction initiation schedule is included in General Condition 154.

In addition to providing a site-specific Inadvertent Release Contingency Plan, the specifications require that the Subcontractor implement the additional necessary safeguards to minimize the likelihood of a fluid release and management/control should a release occur. This includes having a readily available supply of spill response devices (containment booms, pumps, straw bales, silt fence, sediment logs, sandbags, vacuum trucks, and storage tanks) and any other materials or equipment necessary to contain and clean up inadvertent releases. To maximize protection to sensitive environmental areas these measures shall be pre-positioned at the site, readily available and operational prior to the start of any drilling. If needed, additional spill response measures shall be employed immediately, as secondary measures, in the event of a fluid release.

The workspace layout for HDD materials and equipment will be configured to reduce the likelihood of a release. Final dimensions and equipment layout are to be adjusted based on actual space available and shown on the drawings for each HDD crossing.

4.4 DRILLING FLUIDS MANAGEMENT

As described in the Project EM&CP document, drilling fluid (typically bentonite and water based with selected additives) will be NSF certified and all recycling and reuse regulations will be followed where applicable. The drilling fluid management system and subsequent disposal is the responsibility of the HDD subcontractor performing the HDD. However, the drilling fluid management system and subsequent disposal will adhere to the following requirements:

- Drilling fluid will be processed through an initial cleaning that separates the solid materials from the fluid;
- Solids will be sifted out by a screening apparatus/system and the solids deposited into a roll-off or a dump truck and periodically transported off-site and disposed of at an approved disposal facility determined by the HDD construction subcontractor;
- Drilling fluid that is deemed unacceptable to be reused during construction or left over at the end of drilling will be collected and transferred into a tanker truck for disposal at an approved disposal facility determined by the HDD construction subcontractor;
- Petroleum-based fluids and other potentially hazardous materials associated with drilling operations that are spilled during HDD construction will be contained following the mitigation measures described in the SPCC (Appendix K of the EM&CP) and disposed of at an approved disposal facility as determined by the HDD construction subcontractor and included in the EM&CP;
- Supply of spill containment equipment and measures shall be maintained and readily available around drill rigs, drilling fluid mixing system, entry and exit pits and drilling fluid recycling system, if used, to prevent spills into the surrounding environment. Pumps, vacuum trucks, and/or storage of sufficient size will be in place to contain excess drilling fluid; and,
- Under no circumstances will drilling fluid that has escaped containment be reused in the drilling system.

An overview of the drilling fluid system will be submitted to the Environmental Inspector for approval once determined and prior to any HDD installation activities. The role of the Environmental Inspector is discussed in Chapter 3 of the EM&CP.

4.5 EARLY FLUID RELEASE DETECTION

The HDD method has the potential for seepage or fluid loss into pervious geologic formations that the bore path crosses. This may occur due to the presence of fractures in the rock, low

overburden confinement, or from seepage through porous soils such as coarse gravels or via prior exploratory boreholes. It is important to note that inadvertent releases of drilling fluid can occur even if the down-hole pressures are minimal. Subsurface conditions that could be conducive and lead to inadvertent releases or drill difficulties include:

- Highly permeable soil such as cobbles and gravel;
- Presence of rock joints, solution features, or other subsurface fractures;
- Considerable differences in the elevations of HDD entry and exit points (typically greater than 50 feet);
- Disturbed soil, such unconsolidated fill;
- Soft/weak soils with low overburden confining capacity;
- Low density soils in areas where the HDD bore is relatively shallow;
- Longer bore alignments; and
- The presence of archeological features such as, existing wells, piles and culverts, in close proximity to the HDD bore that may provide a preferential path for the drilling slurry to escape from the bore path.

The risks associated with the above conditions at specific crossings are discussed in Section 9 of this report.

An experienced drill crew is the most effective approach to detecting reaction to drilling fluid seepage prior to a surface release. They can promptly stop the drilling, modify the drilling fluid composition, fluid properties, and pressures to address indications of loss of drill fluid. The HDD Subcontractor is required to utilize experienced drill crews particularly in and adjacent to environmentally sensitive areas. The following factors can be used for identifying the potential for drill fluid release:

- The loss of pressure within the drill hole utilizing a downhole pressure monitoring system;
- A large rapid buildup of pressure within the drill hole utilizing a downhole pressure monitoring system or at the drill rig;
- A substantial reduction in the volume of return fluid (loss of circulation); and
- The lack of drill cuttings returning in the drill fluid

In addition to an experienced drill crew, the HDD Subcontractor will be required to perform periodic (at least twice a day) visual inspection and monitoring of the stream channel bottom and wetlands in the vicinity of the drill bit or reaming bit for signs of an inadvertent release. The Environmental Inspector will monitor the status of each HDD waterbody crossing while construction activities are underway until the crossing has been completed and the stream and stream banks have been restored. In the event of any potential or actual failure of the crossing, the Certificate Holders shall have engaged adequate staff, materials, and equipment to take the necessary steps to prevent or avoid adverse environmental impacts. If visual monitoring indicates a potential release, additional measures such as turbidity measurements and bentonite accumulation measurements both upstream and downstream of the current active location of the drill bit are required.

5.0 INADVERTENT RELEASE MONITORING AND NOTIFICATIONS

The HDD Subcontractor is responsible for monitoring of the drilling operation to detect a potential inadvertent release by observing and documenting the flow characteristics of drilling fluid returns to the HDD entry/exit pits and by visual inspection along the drill path. If drilling fluid to the HDD entry/exit pits are lost, the Subcontractor shall implement the following steps:

- The Drill Operator will monitor and document pertinent drilling parameters and conditions and observe and monitor the drill path for evidence of an inadvertent release, if there is evidence (typically visual) of a release, the Subcontractor will be required to stop the drilling immediately;
- The Subcontractor shall notify the lead Environmental Inspector of any significant loss of drilling fluid returns at the drill rig; and, in the event of a detected release of drilling fluid during the performance of any HDD waterbody crossing, implement the procedures specified in the approved EM&CP. The Certificate Holders shall immediately notify New York State Department of Public Service (NYSDPS) Staff and New York State Department of Environmental Conservation of details of the release and the course of action they recommend taking.
- The subcontractor will take steps to modify the drill fluid properties and pressures to reduce the potential of drill fluid loss or release; and
- The Drill Operator will take steps to restore drilling fluid circulation in accordance with the requirements of the HDD technical specifications.

If a fluid release is identified, an immediate response is necessary and the Subcontractor is

required to take proper corrective actions to minimize impacts, particularly to environmentally sensitive resources (e.g. watercourse, waterbodies, and wetlands).

6.0 INADVERTENT RELEASE RESPONSE (UPLAND AND ROAD AREAS)

A common reason for upward movement and release of drill fluid is from borehole collapse or blockage and a resulting increase in the pressure exerted by drill pumps. Lowering drill fluid pressure is a first step to limiting the extent of a release and can be accomplished by stopping drill rig pumps and allowing pressure to bleed off. With no pumping pressure in the hole, surface seepage will generally stop immediately, then the Subcontractor can trip the drill steel back a selected distance and attempt to clear cuttings from the annulus to re-establish circulation.

The HDD Subcontractor will be required to contain/isolate and remove any fluid that has escaped to the ground or mudline surface. On land this can be done through use of berms, straw bales, shovels as needed, or silt fence to contain the release in conjunction with excavating a small sump pit and/or use of vacuum collection equipment, if needed. Sufficient spill-absorbent material will also be required on-site.

If a release is identified in an upland area, the Subcontractor will be required to respond immediately as described above to limit the extents of the release. After containment is established, cleanup and removal can be conducted by hand, with vacuum trucks, or other equipment. The Environmental Inspector will be present during clean up and removal activities, as they may need to be conducted outside of the pre-authorized temporary workspace areas. The Environmental Inspector, Construction Manager, and the HDD Subcontractor will work together closely to determine the best course of action for inadvertent releases occurring within upland areas.

Upon containment of the release, the HDD Subcontractor will be required to evaluate the cause of the seepage and develop mitigation strategies to limit the likelihood of recurrence. The location of the seepage and the area around the seep will be monitored upon the re-start of the HDD operations for changes in conditions. The segments of borehole nearest the entry and exit points and other areas of low overburden cover tend to be the most susceptible to surface seepage as they have the least amount of soil confinement. These locations will generally be in areas of dry land where seepage detection is easily identified and contained. If areas of high risk for inadvertent releases are identified during the HDD design phase, they can be protected from an uncontrolled release through use of strategically placed confinement/filter beds, straw bales, silt fence, or earth berms place prior to the start of drilling or the use of conductor conduits if at entry and exit areas.

7.0 INADVERTENT RELEASE RESPONSE (WETLAND, RAILROAD, AND OPEN WATER BODY AREAS)

For any release occurring in a waterbody, the Certificate Holders shall immediately notify DPS Staff and NYSDEC of details of the release and the course of action they recommend taking. During the performance of any HDD waterbody crossing, contractors monitor the use of an approved drilling solution and, in the event of a detected release of fluid, implement the procedures specified in the approved EM&CP. If an inadvertent release occurs when working beneath the waterway, wetland, or railroad the HDD Subcontractor will be required to cease drilling operations and reduce pressures in borehole immediately, and notify the Environmental Inspector, the Railroad (if within railroad property), the construction management team and the Certificate Holders. The Environmental Inspector, with input from the Drill Operator, will evaluate the potential impact of the release on a site-specific basis and will determine the appropriate course of action. Prior to construction, the HDD Subcontractor is required to develop a detailed, site-specific submittal for general in-stream or in-rail response methods and pre-place necessary materials and equipment at or near the site prior to construction. Specific response actions will be determined in consultation with the Environmental Inspector and HDD Subcontractor and could include the following:

- Shutting down or slowing the drill fluid pumps;
- Modifying the drill fluid properties, add agents to reduce drilling fluid pressures and/or to plug/seal release path;
- Tripping the drill steel back a selected distance and attempt to clear cuttings from the annulus to re-establish circulation
- Stopping drilling activities for 24 hours to allow the bentonite in the subsurface pathways to gel and seal the pathways;
- Evaluate the current drill methods to identify site specific improvements to lower the risk of additional inadvertent releases and,
- Implementation of proper in-wetlands and in upland, road and railroad, handplaced sedimentation control measures including, but not limited to straw bales, vacuum trucks, silt curtains, containment cells, turbidity curtains, or if suitable, sand bags and confinement/filter beds. These activities will require that qualified construction personnel and other support equipment, and supplies be prepositioned and readily available at or near the site.

• Use of a relief well installed at the location of the release. A well or pit equipped with a subsurface pump to control slurry pressures and future releases at that location by evacuating drilling fluid as it accumulates can also be used. The relief well can be utilized to immediately lower the borehole pressures in the event of an inadvertent release and later to control and manage the release as the drilling continues.

8.0 DRILL HOLE ABANDONMENT PLAN

In the event the HDD Subcontractor must abandon the drilled hole, a plan to fill the abandoned hole will be implemented as detailed in the HDD Subcontractor's supplemental Inadvertent Release Contingency Plan and an alternative plan/alignment for crossing shall be evaluated. If it becomes necessary to abandon a partially completed hole, the abandoned hole will be filled with a mixture of high-yield bentonite, water, and drill spoil. The first ten feet of the bore path will be compacted and filled with soil or a cement-bentonite mix to prevent future settlement. The Subcontractor submitted site-specific abandonment plan shall be approved by the Design Engineer and the Construction Manager prior to being performed in the field.

After the abandoned hole has been filled, an alternative entry and exit hole and bore path alignment will be evaluated by the HDD Subcontractor, Construction Manager, and the Design Engineer. The new alignment shall be offset from the abandoned hole by at least 10 feet (except at the ends where a 5- foot offset may be used) to help limit the risk of steering difficulties due to the presence of a hydraulic connection causing drill fluid loss to the abandoned hole.

9.0 CROSSING SPECIFIC DISCUSSION

9.1 HDD CROSSING #1 – LAKE ROAD

HDD #1 consists of two, straight (in plan view) HDD bores, each approximately 896 and 881 feet long as shown in Appendix C. The HDD bores will pass approximately 29 to 32 feet below the bottoms of a pair of 12-foot-diameter culverts stream which conduct the Mill Brook under Lake Road. The approximate center of the HDD bores located under the culverts at latitude 43.7222°N and longitude -73.4182°W, in Putnam, NY. The ground surface elevations along the path of HDD #1 gently undulates between approximately El. 266 and El. 292 (reference datum NAVD 1988). Waterbodies and wetlands are present between approximately Sta. 10147+60 and Sta. 10148+60 (at about El. 268) and between approximately Sta. 10152+80 and Sta. 10153+25 (at about El. 276).

The bores will have no horizontal curves. The vertical curves of the bore path are designed so that the bore will pass beneath Lake Road and the culverts under Lake Road. The proposed work at this location must be constructed in accordance with the Article VII Certificate and associated EM&CP.

<u>Ground conditions at HDD #1</u> - Borings GTB-PD7 & GTB-PD7A are located along the proposed HDD alignment between approximately Sta. 10146+50 and Sta. 10148+00. These two [2] ranged

in depth to approximately 50 feet and are shown on Appendix C. Based on the borings, the soil profile for the HDD #1 BoreAid analyses was divided into two [2] layers: medium dense silt and very soft to soft lean clay. The soil profiles used for BoreAid analyses of the HDDs in this segment are shown in Appendix A.

Specific design considerations for HDD #1 include:

- General depth of soil cover under the culverts and the adjacent Mill Brook is 26 to 32 feet near the centers of the bore paths. Preliminary analysis of the bores indicates the lowest maximum allowable pressure capacity in the middle of the bores to be approximately 45 psi. The total circulating pressure estimated to occur in the middle of the bore ranges from 34 to 42 psi assumed standard HDD drilling methods. In the remainder of the bore the maximum allowable pressure ranges from approximately 0 to 80 psi and the approximate applied slurry pressure during drilling ranges from 0 to 42 psi. A sketch showing the maximum allowable pressure and the applied pressure is provided in the summary BoreAid analyses in the attached Appendix A.
- It appears that a potential for releases at the starting and ending 10-20 feet near the exit pits exist. These should be relatively easily controlled through the use of conductive conduit, straw bales, silt fences, erosion control measures and vacuum trucks.
- The entry and exit points are established outside the wetland or waterway boundary to permit detection and response, in the event of a release, before environmentally sensitive boundaries are reached or impacted. Erosion and sediment control measures will be placed between the entry/exit location and any watercourses, waterbodies, and environmentally sensitive areas as an additional precaution.

In our opinion the conditions conducive to inadvertent releases that may exist this at this site based on the ground conditions described in the borings at the site include:

- Highly permeable soil such as cobbles and gravel in the stream bottom In our opinion, based on the geomorphology of the area, the presence of sufficient highly permeable soils of sufficient thickness is not likely and the risk of a release due to this condition is low.
- Soft soils with low overburden capacity encountered in the borings The borings

indicate that 5 feet of clay immediately below the culverts is a medium stiff to stiff clay which combined with the depth of the bores below the culverts and the results of the BoreAid analyses leads to our opinion that the risk of a release due to this condition is low also.

9.2 HDD CROSSING #2 – SOUTH BAY

HDD #2 consists of two, curved (in plan view) HDD bores located under the Champlain Canal-South Bay, south of the State Route 22 bridge across the canal. The bores are approximately 2989 and 3032 feet long as shown Appendix C. The HDD bores will pass approximately 54 to 55 feet below the low mudline of the canal. The horizonal alignment of HDD #2 was revised from north of the bridge to south of the bridge to avoid archeological ruins in bottom of the canal and to avoid deep (up to 95 feet deep) deposits of rock fill that were place in the bottom of the canal in unsuccessful attempts to support two earlier bridges located north of the current bridge. The rock fill is generally not compatible with the HDD method of construction and if encountered, creates a greater risk for inadvertent releases. The approximate center of the HDD bores under the Champlain Canal-South Bay are at latitude 43.5425°N and longitude - 73.4314°W, in Whitehall, NY. The ground surface elevations along the path of HDD #2 ranges from approximately El. 125 at the west end of the bore alignment, to approximately Elevation 82 at the mudline in the middle of the canal, to El. 120 at the east end of the bore alignment (reference datum NAVD 1988). Approximately 1500 feet of the bore alignment will be under the waters of the Champlain Canal – South Bay.

The bores will have both horizontal and vertical curves, but no segments of the bore path are designed with compound curves (segments with compound curves would have both horizontal and vertical curves). The design curves for both the horizontal and vertical paths of the alignment have a minimum radius of approximately 1000 feet to limit steering issues in the soft soils at this site.

The proposed work at HDD #2 will be located underneath the South Bay of the Champlain Canal and adjacent wetlands and uplands. No work is proposed within the water body. Both work zones are adjacent to wetlands, but have been configured to avoid them as much as possible. Steps must be taken to protect and limit disturbance to the wetlands, and to restore the wetlands after the

HDD work is completed should they be disturbed. The proposed work at this location must be constructed in accordance with the Article VII Certificate and associated EM&CP.

The Certificate Holders have received permits for the project including a modified Section 404 permit from the USACE.

<u>Ground conditions at HDD #2</u> - Based on borings drilled for this project and historic borings for the State Route 22 bridge construction, the soil profile the for HDD #2 BoreAid analyses was divided into four [4] layers: Loose Silt, Upper Soft Clay, Medium Stiff Clay, and Lower Soft Clay. The Rock Fill encountered during recent borings from the existing causeway is not expected to be present along the south of Bridge alignment selected. The soil profiles used for BoreAid analyses of the HDDs in this segment are presented in Appendix A.

Archeological ruins and remains of old bridges were noted north of the bridge at HDD #2. Remains of approximately 10 sunken ships or barges, some circa 1812, and a 1913 bridge are located just north of the jetties, see Appendix B. In addition, the records appear to indicate that barges were sunk as part of the foundation system for the 1913 bridge in addition to dumpling gravel, cobbles and boulders and pushing them down into the soft sediments. The locations of these ruins and related obstructions are not expected to be present along the south of bridge alignment selected as shown in the recent geophysical survey report as discussed in the Design Summary Report.

Specific design considerations for HDD #2 include:

- Depth of cover during profile design (based on soil borings) to limit the potential inadvertent break through to the water body, road, wetlands, or ground surface. General depth of cover under the Canal mulline is 50 or more feet with a depth of cover of about 54 feet near the center of the bore path. Preliminary analysis of the bore, assuming typical drilling methods, indicates that the lowest maximum allowable pressure capacity in the middle of the bore is approximately 68 psi and the pressure estimated to occur in the bore in the middle portion ranges from 75 to 70 psi assumed standard HDD drilling methods. In the remainder of the bore the maximum allowable pressure ranges from approximately 0 to 80 psi and the approximate applied slurry pressure during drilling ranges from 0 to 71 psi. A sketch showing the maximum allowable pressure and the applied pressure is provided in the summary BoreAid analyses in the attached Appendix A.
- It appears that a potential for releases in the last 300 to 400 feet of the bores near as each

bore approaches the exit pit exist, regardless of the direction of the bore E-W or W-E. This is related to the length and depth of the bores and the slope of the ground surface up from the water's edge to the entry and exit pits about 30 feet higher.

- Generally, for the formation of inadvertent releases, the more critical stage of the HDD process tends to be during the initial pilot hole drilling when the annular space between the bore sidewall and the drill string is the smallest.
- Adjusting the drill alignment to miss existing infrastructure including existing utilities, and other obstacles,
- Establishing a drill alignment line that allows for gradual angular changes to minimize pressure build-up,
- Requiring drilling fluid composition and drilling procedures that minimize drilling fluid pressures,
- Requiring drilling fluids that adequately address site-specific drilling concerns while posing the least threat to the environment,
- Requiring monitoring and controlling drilling fluid pressures with down-the-hole sensors during pilot hole drilling,
- Requiring the use of intersect bore method (drilling the pilot bore from each end and meeting in the middle) to reduced slurry pressures at the exit end during pilot bore drilling, thereby reducing the potential for a released at the exit end of the pilot bore, and
- The use of conductor conduits, temporary steel conduit approximately 30 inches diameter and 100 feet long at each end of each bore to contain drilling fluids during drilling reaming and pullback.

Appendix A

BoreAid HDD Simulation Output



Generated Output

WARNING: The accuracy of the data obtained by the BoreAid® system is highly dependent upon accurate data gathering, data input and proper use of the software. Vermeer is not responsible for that information. BoreAid® data is not intended to replace the need for future on-site utility locating, measuring and verification procedures, which are essential for accurate placement of new underground installations and avoidance of existing utilities.

CALL YOUR ONE-CALL SYSTEM FIRST

WARNING: Always contact your local One-Call system before the start of your digging project. The BoreAid® system is intended to be used with other utility locating methods, such as the use of the One-Call system and the exposing of existing utilities by potholing.

Locate utilities before drilling. Call 811 (U.S. only) or 1-888-258-0808 (U.S. or Canada) or local utility companies or national regulating authority.

Before you start any digging project, do not forget to call the local One-Call system in your area and any utility company that does not subscribe to the One-Call system. For areas not represented by One-Call Systems International, contact the appropriate utility companies or national regulating authority to locate and mark the underground installations. If you do not call, you may have an accident or suffer injuries; cause interruption of services; damage the environment; or experience job delays.

OSHA CFR 29 1926.651 requires that the estimated location of underground utilities be determined before beginning the excavation or underground drilling operation. When the actual excavation or bore approaches an estimated utility location, the exact location of the underground installation must be determined by a safe, acceptable and dependable method. If the utility cannot be precisely located, it must be shut off by the utility company.

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Description:	Designer:	General:
Lake Road HDD - New York	TAR CHA	HDD #1 Ref: Lake Road - New York P1A Start Date: 12-10-2021 End Date: 12-10-2021

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Input Summary

(0.00, 0.00, 0.00) ft	Drill Rig Location
3.5 in	Rod Diameter
15.00 ft	Rod Length
1.19 in	Pipe Thickness
9.0	Pipe DR
10.750 in	Pipe OD
IPS	OD Classification
HDPE	Pipe Type
884.00 ft	Project Length
(884.00, 0.00, 289.76) ft	End Coordinate
(0.00, 0.00, 291.00) ft	Start Coordinate

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Soil Summary

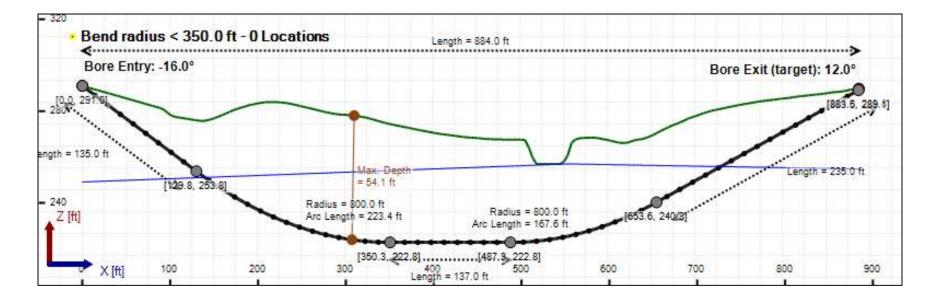
Number of Layers: 2

Soil Layer #1 USCS, Silt (M), ML From Assistant Unit Weight: 0.0521 (dry), 0.0637 (sat) [lb/in3] Phi: 32.00, S.M.: 100.00, Coh: 0.00 [psi]

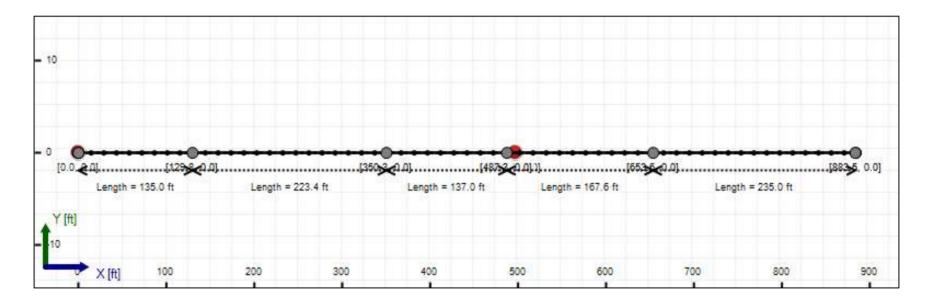
Soil Layer #2 USCS, Clay (C), CL From Assistant Unit Weight: 0.0405 (dry), 0.0579 (sat) [lb/in3] Phi: 0.00, S.M.: 200.00, Coh: 3.13 [psi]

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Bore Cross-Section View







Load Verifier Input Summary:

Ballast Unit Weight: 0.03613 lb/in3 Hydrokinetic Pressure: 10 psi Slurry Unit Weight: 0.05419 lb/in3 Pipe-soil friction angle: 30 Surface-pipe friction coefficient in borehole: 0.3 Surface-pipe friction coefficient at entrance: Allowable Compressive Stress (Short Term): 1150 psi Allowable Tensile Stress (Long Term): 1100 psi Allowable Tensile Stress (Short Term): 1200 psi Pipe Unit Weight: 0.03430 lb/in3 Short Term Poisson Ratio: 0.35 Short Term Modulus: 57500 psi Surface Surcharge: 0 psi Silo Width: 1.34400002161662 ft Borehole Diameter: 1.34400002161662 ft Internal Pressure: 0 psi Pipe Length: 899.99 ft Pipe DR: 9 Pipe OD: 10" (10.75") Classification: IPS Pipe Type: HDPE Pipe Application: Electrical Cable Allowable Compressive Stress (Long Term): 1150 psi Long Term Poisson Ratio: 0.45 Long Term Modulus: 28200 psi 0.5

In-service Load
ad
Summary:

Compressive Stress [psi]	Reissner Effect0Net Deflection1.371	Deflection Earth Load Deflection 1.239 Buoyant Deflection 0.132	Internal Pressure0.0Net Pressure18.5	Water Pressure14.4Surface Surcharge0.0	Pressure [psi] Deformed Earth Pressure 4.1
162.2	0	6.782	0.0	12.8	Collapsed
	6.914	0.132	36.0	0.0	23.2

Installation Load Summary:

Forces/Stresses	@Maximum Force	Absolute Maximum
Pullback Force [lb]	17030.0	17030.0
Pullback Stress [psi]	474.9	474.9
Pullback Strain	8.260E-3	8.260E-3
Bending Stress [psi]	0.0	32.2
Bending Strain	0	5.599E-4
Tensile Stress [psi]	474.9	505.4
Tensile Strain	8.260E-3	9.349E-3

Net External Pressure = 34.2 [psi] Buoyant Deflection = 0.1

Hydrokinetic Force = 567.6 lb

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Deflection [%] Unconstrained Collapse [psi] Compressive Wall Stress [psi]	Calculated 1.371 44.0 83.2	Allowable 7.5 123.4 1150.0	Factor of Safety 5.5 2.8 13.8	Check OK OK OK
Compressive Wall Stress [psi]	83.2	1150.0	13.8	OK
Installation Analysis	Calculated	Allowable	Factor of Safety	Check

•				
	Calculated	Allowable	Factor of Safety	Check
Deflection [%]	0.065	7.5	115.8	OK
Unconstrained Collapse [psi]	54.3	227.5	4.2	OK
Tensile Stress [psi]	505.4	1200.0	2.4	OK

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Maximum Allowable Bore Pressure Summary

Ream Number	Initial Diameter	Final Diameter	Estimated Maximum Pressure (Avg.)	Estimated Maximum Pressure (Local)
Pilot Bore	0.00 in	8.00 in	79.569 psi	59.712 psi
1	8.00 in	12.00 in	79.537 psi	59.621 psi
2	12.00 in	16.13 in	79.492 psi	59.489 psi

Note: The maximum bore pressures presented in this table are the maximum values along the length of the bore and not the maximum allowable at any point. The estimated maximum pressures should be compared to the estimated circulating pressures along the bore to determine potential locations of inadvertant returns.

Estimated Circulating Pressure Summary

Active	Shear Rate [rpm]	Shear Stress [Fann Degrees]
No	600	37
No	300	32
No	200	29
Yes	100	25
Yes	6	17
No	ω	15

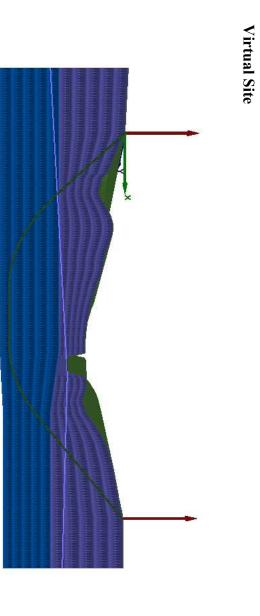
Flow Rate (Q): 40.00 US (liquid) gallon/min

Drill Fluid Density: 0.040 lb/in3

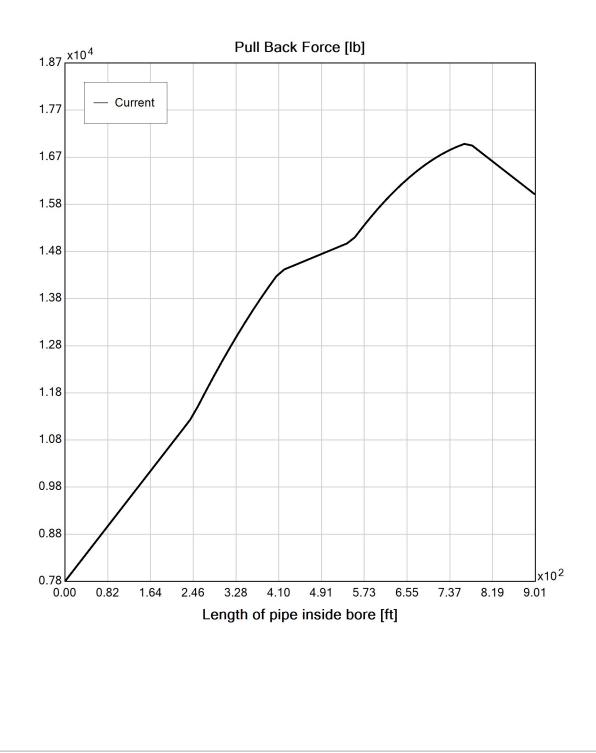
Rheological model: Bingham-Plastic Plastic Viscosity (PV): 25.53

Yield Point (YP): 16.49

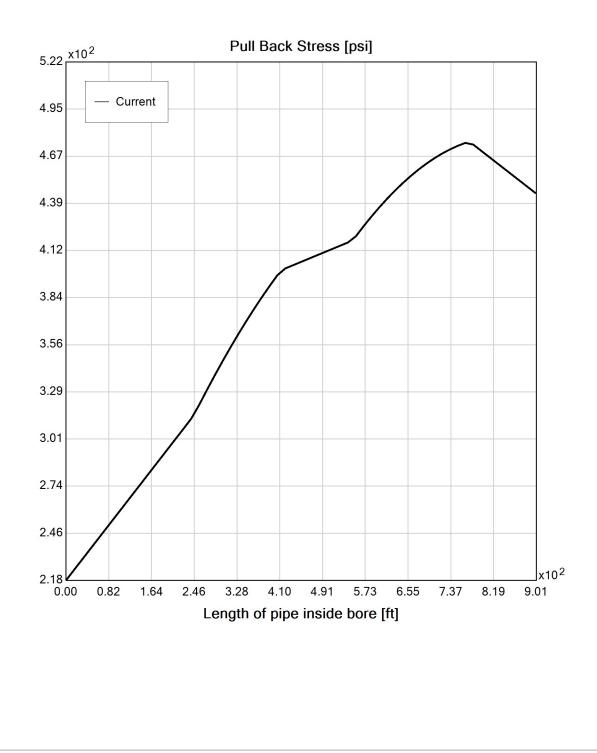
Effective Viscosity (cP): 1202.0



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